## Protection Devices -

Miniature Circuit Breakers

The new range of miniature circuit breakers offer increased performance over the previous range. They conform to BS EN 60947-2 standard and can be used to switch on every type of load.

They offer increased safety with an IP2X rating on the screw and terminals.

Other new features include:

- The new terminal architecture transfers all of the tightening torque directly on to the terminal cage and wire.
- Totally new tripping mechanism wth a snap close system.
- Better breaking performance characteristics.
- Circuit labelling window.
- Easily removable from the din rail with top and bottom removable clips.



| Miniature circuit breakers 6kA type B SP | 3.2 |
| :---: | :---: |
| Miniature circuit | 3.3 |
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| 630A frame MCCBs accessories and auxili | $\begin{aligned} & 3.31 \\ & \text { ies } \end{aligned}$ |

## Miniature Circuit Breakers

6kA Type B SP - MTN


MTN140

| NBNxxxA : "B" Curve | Description | Control | Connection capacity |
| :--- | :--- | :--- | :--- |
| NCNxxxA : "C" Curve | These MCBs allow you to ensure | With a fast system of closing, | - 25mm ${ }^{2}$ flexible conductor |
| NDNxxxA : "D" Curve | - Protection of circuits against | we increase the withstand of | - 35mm |
|  | short circuits conductor |  |  |


|  | Designation | $\mathrm{In} / \mathrm{A}$ | Width in 17.5 mm | Pack qty | Cat ref. "B" Curve | "C" Curve | "D" Cruve |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Single Pole MCB | 0.5 | 1 | 12 |  | NCN100A | NDN100A |
| 12-0 | $\star$ | 1 | 1 | 12 |  | NCN101A | NDN101A |
| - | - | 2 | 1 | 12 |  | NCN102A | NDN102A |
|  |  | 3 | 1 | 12 |  | NCN103A | NDN103A |
|  |  | 4 | 1 | 12 |  | NCN104A | NDN104A |
|  |  | 6 | 1 | 12 | NBN106A | NCN106A | NDN106A |
| - 8 |  | 10 | 1 | 12 | NBN110A | NCN110A | NDN110A |
| NCN116A |  | 13 | 1 | 12 | NBN113A | NCN113A | NDN113A |
|  |  | 16 | 1 | 12 | NBN116A | NCN116A | NDN116A |
|  |  | 20 | 1 | 12 | NBN120A | NCN120A | NDN120A |
|  |  | 25 | 1 | 12 | NBN125A | NCN125A | NDN125A |
|  |  | 32 | 1 | 12 | NBN132A | NCN132A | NDN132A |
|  |  | 40 | 1 | 12 | NBN140A | NCN140A | NDN140A |
|  |  | 50 | 1 | 12 | NBN150A | NCN150A | NDN150A |
|  |  | 63 | 1 | 12 | NBN163A | NCN163A | NDN163A |
|  | Double Pole MCB | 0.5 | 2 | 6 |  | NCN200A | NDN200A |
|  | $\begin{aligned} & * \\ & \{ \end{aligned}$ | 1 | 2 | 6 |  | NCN201A | NDN201A |
|  |  | 2 | 2 | 6 |  | NCN202A | NDN202A |
|  |  | 3 | 2 | 6 |  | NCN203A | NDN203A |
|  |  | 4 | 2 | 6 |  | NCN204A | NDN204A |
|  |  | 6 | 2 | 6 | NBN206A | NCN206A | NDN206A |
|  |  | 10 | 2 | 6 | NBN210A | NCN210A | NDN210A |
| NCN216A |  | 13 | 2 | 6 | NBN213A | NCN213A | NDN213A |
|  |  | 16 | 2 | 6 | NBN216A | NCN216A | NDN216A |
|  |  | 20 | 2 | 6 | NBN220A | NCN220A | NDN220A |
|  |  | 25 | 2 | 6 | NBN225A | NCN225A | NDN225A |
|  |  | 32 | 2 | 6 | NBN232A | NCN232A | NDN232A |
|  |  | 40 | 2 | 6 | NBN240A | NCN240A | NDN240A |
|  |  | 50 | 2 | 6 | NBN250A | NCN250A | NDN250A |
|  |  | 63 | 2 | 6 | NBN263A | NCN263A | NDN263A |


| NBNxxxA : "B" Curve | Description | Control | Connection capacity |
| :--- | :--- | :--- | :--- |
| NCNxxxA : "C" Curve | These MCBs allow you to ensure | With a fast system of closing, | - 25mm ${ }^{2}$ flexible conductor |
| NDNxxxA : "D" Curve | - Protection of circuits against | we increase the withstand of | - 35mm |
|  | short circuits conductor |  |  |



## Auxiliaries and Accessories for Devices NBN, NCN, NDN, 10kA MCBs



## RCCB add-on blocks for MCB devices NBN, NCN, NDN






2 pole MCB and add on block showing unique sliding connection feature
hager

The new range of modular protection devices ranging from 80 to 125A re-inforces Hagers commitment to new product development in protection solutions for OEMs and commercial buildings.

Especially designed to provide :

- Protection as main incomer for sub distribution
- Protection of loads directly supplied by a distribution board.

Offering benefits focussed on safety, ease of installation and use friendliness, this is another example by Hager of continuous investment to develop products for the future.



The HM range of MCBs and addon blocks benefit from the new exclusive "cage connection".


The connection of auxiliaries becomes easy, thanks to the new "Fast on" connection terminals provided on the to and bottom of the MCBs. This provided a quick and easy solution to feed auxiliaries such as shunt trip coil, UV release etc.

Capacity:

- 1.5 to 6mm²
- Maximum current 6A


Across the range, the assembly of the add-on block is carried out in three simple steps.

1. Assembly
2. Conneciton
3. Locking


| Miniature Circuit <br> Breakers 80-125A | 3.10 |
| :--- | :--- |
| HMF "C" Curve | 3.11 |
| HMF "C" Curve 15kA | 3.12 |
| HMD "D" Curve 15kA | 3.13 |
| RCD Add-on Blocks <br> type AC | 3.14 |



The add-on blocks are available in fixed and adjustable versions. In adjustable version, the sensitivity and the time delay can be adjusted, even when connected.


The RCD Add on block is equipped with locating pins which helps to secure the tightening of the bottom terminals to the circuit breaker. The cover cannot be closed if the terminals are not tightened correctly


The MCBs can lock in "OFF" position by the integrated locking facility on the toggle.

This lock allows inserting a 2,5 to $3,5 \mathrm{~mm}$ plastic cable tie where you can fit a warning card if necessary (delivered with each product).


The DIN rail clips of the circuit breaker unit and add-on-block facilitate its mounting. They are easily accessible with a screwdriver.


Series HMC, HMD, HMF :

These circuit breakers are equipped with reinforced screw cages.

A label holder is integrated under the toggle to ensure the location of the product

The "OFF" position is clearly shown by a green indicator below the toggle.

Suitable for isolation (according to BS EN 60947-2) : the isolation of the circuit breakers is indicated by a green indicator on the toggle.

These circuit breakers have quick closing : fast and simultaneous closing of the contacts, independent of the handling speed.
This increases the life of the circuit breaker whatever the type of load.

Nominal voltage : 230/415 V ~ calibration setting :30 ${ }^{\circ} \mathrm{C}$
(BS EN 60898-1) insulation voltage: 500 V

## Options :

$\square$ auxiliary :

- to visualise the state ON or OFF of the circuit breaker, - to ON/OFF remotely the circuit breakerlocking mechanism
$\square$ terminal covers and phase separatorsRCD add-on blocks

| Model | Icc/Curve | Accessories | Fast-on <br> connection | Tightening <br> comp. system | Lockable <br> handle | Front product <br> labelling |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| HMF | 10kA / C | YES | NO | NO | NO | YES |
| HMC / HMD | 15kA / C, D | YES | YES | YES | YES | YES |

Miniature Circuit Breakers 80-125A

| Curves "C" | 10 kA (BS EN 60898-1) 10 kA (BS EN 60947-2) | Tripping curves <br> "C" magnetic setting between 5 and 10 ln . | Connection capacity <br> - $35 \mathrm{~mm}^{2}$ flexible wire $\left(50 \mathrm{~mm}^{2}\right.$ <br> possible with some cable end-caps), | KEMA approved according to BS EN 60898-1, BS EN 947-2 standards. |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Use: | - $70 \mathrm{~mm}^{2}$ rigid wire |  |
| In 80 to 125 A |  | Commercial and industrial applications |  |  |



HMF199T


HMF299T


HMF399T

HMF499T

| Circuit breakers 4 poles | 80 | 6 | HMF480T |
| :--- | :--- | :--- | :--- |
|  | 100 | 6 | HMF490T |
|  | 125 | 6 | HMF499T |


| Designation | In/A | Width in <br> 17.5 mm | Cat Ref. <br> "C" Curve |
| :--- | :--- | :--- | :--- |
| Circuit breakers 1 pole | 80 | 1.5 | HMF180T |
|  | 100 | 1.5 | HMF190T |
|  | 125 | 1.5 | HMF199T |


| Circuit breakers 2 poles | 80 | 3 | HMF280T |
| :--- | :--- | :--- | :--- |
|  | 100 | 3 | HMF290T |
|  | 125 | 3 | HMF299T |


| Circuit breakers 3 poles | 80 | 4.5 | HMF380T |
| :--- | :--- | :--- | :--- |
|  | 100 | 4.5 | HMF390T |
|  | 125 | 4.5 | HMF399T |

125
HMF499T


Miniature Circuit Breakers 80-125A

| Curves "C" | 15 kA <br> (BS EN 60898-1) <br> 15 kA <br> (BS EN 60947-2) | Tripping curves <br> "C" magnetic setting between 5 and 10 ln . | Connection capacity - $35 \mathrm{~mm}^{2}$ flexible wire $\left(50 \mathrm{~mm}^{2}\right.$ possible with some cable end-caps), | KEMA approved according to BS EN 60898-1,BS EN 947-2 standards. |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Use : | - $70 \mathrm{~mm}^{2}$ rigid wire |  |
| In 80 to 125 A |  | Commercial and |  |  |



| Designation | In/A | Width in I <br> 17.5 mm | Cat Ref. <br> "C" Curve |
| :--- | :--- | :--- | :--- |
| Circuit breakers 1 pole | 80 | 1.5 | HMC180T |
|  | 100 | 1.5 | HMC190T |
|  | 125 | 1.5 | HMC199T |

HMC199T


| Circuit breakers 2 poles | 80 | 3 | HMC280T |
| :--- | :--- | :--- | :--- |
|  | 100 | 3 | HMC290T |
|  | 125 | 3 | HMC299T |


| Circuit breakers 3 poles | 80 | 4.5 | HMC380T |
| :--- | :--- | :--- | :--- |
|  | 100 | 4.5 | HMC390T |
|  | 125 | 4.5 | HMC399T |



HMC499T

Miniature Circuit Breakers 80-125A


|  | Designation | $\mathrm{In} / \mathrm{A}$ | Width in 17.5 mm | Cat Ref. "C" Curve |
| :---: | :---: | :---: | :---: | :---: |
|  | Circuit breakers 1 pole | 80 | 1.5 | HMD180T |
|  |  | 100 | 1.5 | HMD190T |
|  |  | 125 | 1.5 | HMD199T |
| HMD299T | Circuit breakers 2 poles | 80 | 3 | HMD280T |
|  |  | 100 | 3 | HMD290T |
|  |  | 125 | 3 | HMD299T |
|  | Circuit breakers 3 poles | 80 | 4.5 | HMD380T |
| HMD399T |  | 100 | 4.5 | HMD390T |
|  |  | 125 | 4.5 | HMD399T |
| $1-2$ | Circuit breakers 4 poles | 80 | 6 | HMD480T |
|  |  | 100 | 6 | HMD490T |
| HMD499T |  | 125 | 6 | HMD499T |

Accessories for Circuit Breakers

|  | Designation | Characteristics | Cat Ref. |
| :--- | :--- | :--- | :--- |
| MZN 130 | Terminal covers / Screw cap | Allows to cover connection terminals, <br> screws of circuit breakers. The screw <br> covers can be sealed. | MZN130 |
|  | Phase separator | 1 set of 3 phase separators | MZN131 |

MZN 131

## RCD add-on blocks type AC $\sim$ <br> for circuit breakers HMC, HMD, HMF

RCD add-on blocks for circuit breakers HMC, HMD, HMF.

## Fixed :

- high sensitivity 30 mA instantaneous
- low sensitivity 300 mA instantaneous.


## Settings :

- sensitivity I $\Delta$ n 0,3-0,5-1 A ...
- delay $\mathrm{S} \Delta \mathrm{t} 0$ - $60-150 \mathrm{~ms}$.

These devices are intended to be fixed on the right side of the circuit breakers to form differential circuit breakers from 80 to 125A, two, three or four-pole.

This "circuit breaker + block" ensures, in addition to the overload and short circuit protection, the protection of the installations against the insulation defects $(300 \mathrm{~mA}$ and 1 A ) and the protection of the people against the direct contacts ( 30 mA ) and indirect ( 300 mA ).

## Adjustable blocks :

the setting is done by actuating the thumbwheel in front face. The setting thumbwheels are protected by a transparent sealable cover.

## Disassembly :

the bistable latch (2 positions) facilitate the assembly or disassembly by the bottom of the "circuit breaker + block."

These RCD add-on blocks exist in version AC and in version A-HI.

Version AC ~:
the add-on blocks are protected against unexpected tripping caused by the transitory leakage currents : lightning, capacitive loading.

High Immunity :
The products with "reinforced immunity" reduce the unexpected tripping when they protect equipment generating disturbances (micro-processing, electronic ballast,...)

The earth fault is indicated when the handle is in lower position (yellow colour).
Test button for earth fault check.

Tightening compensation

## cages

These circuit breaker blocks are equipped with screw cages with tightening compensation, reinforcement arch and cable holding jaws. These elements contribute to an effective tightening over time.

## Connection capacity :

- $35 \mathrm{~mm}^{2}$ flexible connection ( $50^{\circ}$
possible with some terminals),
- $70 \mathrm{~mm}^{2}$ rigid connection.

Assembly and disassembly facilitated by the drawer assembly system. The terminal cover is dependent of the add-on block. It is provided with keying systems avoiding the omission of terminal tightening downstream of the circuit breaker. .

Nominal voltage : -15 +10 \%
2 poles : 230 V
three and four-pole : 230/400 V test button : 230/400 V.

In conformity with the requirements of the appendix $G$ of the BS EN 61009-1. In conformity with the requirements of standard BS EN 60947-2.


BTC 280E


BDC 480E

association circuit breaker + add-on block 4 poles adjustable


## Single Pole and Switched Neutral (SPSN) Devices <br> - MCB and Fuse Carrier




MLN710A


MLN740A

| Designation | Current <br> (A) | Width in II | Pack <br> qty | Cat Ref. |
| :--- | :--- | :--- | :--- | :--- |
| MCB <br> Single Pole \& Switched Neutral | 6 | 1 | 12 | MLN706A |
|  | 10 | 1 | 12 | MLN710A |
|  | 16 | 1 | 12 | MLN716A |
|  | 20 | 1 | 12 | MLN720A |
| Fuse Carrier <br> Single Pole \& Switched Neutral <br> without fuse fitted. | 10 | 1 | 12 | MLN732A |
|  | 40 | 1 | 12 | MLN740A |


| Spare fuse type gF <br> $10 A-8.5 \times 23 \mathrm{~mm}$ | 10 | 10 | LF138 |
| :--- | :--- | :--- | :--- |
| 16 A $-10.3 \times 25.8 \mathrm{~mm}$ | 16 | 10 | LF139 |
| 20 A $-8.5 \times 31.5$ | 20 | 10 | LF140 |
| $25 A-10.3 \times 31.5 \mathrm{~mm}$ | 25 | 10 | LF141 |
| $32 A-10.3 \times 38 \mathrm{~mm}$ | 32 | 25 | LF142 |
| Single module blank <br>  <br> blanks spare ways |  |  |  |


| Locking kit | This allows locking of the device | 2 | MZN175 |
| :--- | :--- | :--- | :--- |
| For the toggle of the device. | toggle in the on/off position. |  |  |
| Supplied without padlock. | Will accept two padlocks with |  |  |
| For use with MCCB's. | hasps of 4.75 mm diameter max. |  |  |

## 2 \& 4 Pole RCCBs



## RCCB

- Auxiliaries

|  | Configurations For technical details see page 3.38 . |  | $\bigcirc$ $\bigcirc$ <br>   <br>  $O$ <br> RCCB |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Designation | Description | Width in 17.5 mm | Pack qty. | Cat Ref. |
|  | Interface auxiliary Indicates the position of the associated RCCB On, Off, Tripped. Also acts as RCCB interface with standard MCB auxiliaries MZ203-MZ206 | $\begin{aligned} & \text { 2NO 2NC } \\ & \text { 6A AC1 } 230 \mathrm{~V} \end{aligned}$ | 1 | 1 | CZ001 |
| CZ201 | Shunt trip | Allows remote tripping of the associated device. Operation of the coil is indicated by a flag on the product fascia $230 \mathrm{Vac}-400 \mathrm{Vac}$ <br> $110 \mathrm{~V}-130 \mathrm{Vdc}$ <br> 24-48Vac $12-48 \mathrm{Vdc}$ |  | 1 1 |  |
|  | Under voltage release | Allows RCCB to be closed, only when voltage is above $85 \%$ of Un. RCCB will automatically trip when voltage falls to between 70-35\% of Un (230V). Operation of the release is indicated by a flag on the product facia. |  |  |  |
|  |  | 230 Vac <br> 48 Vdc | $1$ <br> 1 | 1 1 | $\begin{aligned} & \text { MZ206 } \\ & \text { MZ205 } \end{aligned}$ |
|  | Locking kit <br> For the dolly of the device. Supplied without padlock. | This allows locking of the device dolly in the on/off position. Will accept two padlocks with hasps of 4.75 mm diameter max. |  | 2 | MZN175 |

[^0]
## RCBO

- Single Pole

- Single Pole and Switched Neutral



## RCBO

- Single Pole and Switched Neutral Type C 4.5kA


ADC806F

| Designation | In/A | Width in \\| <br> $17.5 m m$ | Pack <br> qty. | Cat Ref. <br> Type "C" |
| :--- | :--- | :--- | :--- | :--- |
| RCBO <br> All terminal version for cable in <br> cable out applications e.g. local <br> protection, caravan pitches, <br> festive illuminations, street <br> lighting. | 10 | 16 | 2 | 1 | ADC806F



BS 88 HRC fuse carriers and fuses


## Motor Starters




MM501N


MZ520N


MZ521N

| Designation | Current setting | standard power ratings of 3 phase motors 50/60Hz (AC3 category) $230 \mathrm{~V}(\mathrm{~kW}) \quad 400 \mathrm{~V}(\mathrm{~kW})$ | Width in 17.5 mm | Pack qty. | Cat Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| motor starters | 0.1-0.16A |  |  | 1 | MM501N |
|  | 0.16-0.25A | 0.06 | $21 / 2$ | 1 | MM502N |
|  | 0.25-0.4A | 0.06 0.09 | $21 / 2$ | 1 | MM503N |
|  | 0.4-0.6A | 0.09 0.12 | $21 / 2$ | 1 | MM504N |
|  | 0.6-1.0A | 0.09 0.12 | $21 / 2$ | 1 | MM505N |
|  | 1.0-1.6A | $0.25 \quad 0.55$ | $21 / 2$ | 1 | MM506N |
|  | 1.6-2.5A | 0.55 0.8 | $21 / 2$ | 1 | MM507N |
|  | 2.5-4A | 0.8 1.5 | $21 / 2$ | 1 | MM508N |
|  | 4-6A | $1.5 \quad 2.5$ | $21 / 2$ | 1 | MM509N |
|  | 6-10A | 2.54 | 2 1/2 | 1 | MM510N |
|  | 10-16A | 47.5 | $21 / 2$ | 1 | MM511N |
|  | 16-20A | 5.59 | $21 / 2$ | 1 | MM512N |
|  | 20-25A | 7.512 .5 | $21 / 2$ | 1 | MM513N |
| Auxiliary contacts <br> (Act as an indicating device to monitor the ON or OFF position) | $1 \mathrm{C}+10$ | $\begin{aligned} & 2 \mathrm{~A} \mathrm{AC1}-400 \mathrm{~V} \sim \\ & 3.5 \mathrm{~A} \mathrm{AC1}-230 \mathrm{~V} \end{aligned}$ | 1/2 | 1 | MZ520N |


| Alarm contact | 1C | 1A AC1-400V $\sim$ | 1 | MZ527N |
| :--- | :--- | :--- | :--- | :--- |
| (Mounted inside the |  | $2 A$ AC1-230V $\sim$ |  |  |

motor starter)

| Under voltage release <br> (To prevent automatic <br> restarting of the <br> controlled device) | $230 \mathrm{~V} \sim 50 \mathrm{~Hz}$ | 1 | MZ528N |
| :--- | :--- | :---: | :---: |
| Surface mounting enclosure | $400 \mathrm{~V} \sim 50 \mathrm{~Hz}$ | 1 | MZ529N |
| w. $78 \mathrm{~mm} \times \mathrm{h} .150 \mathrm{~mm} \times$ d. 95 mm |  |  |  |
| Reatherproof IP55 |  |  |  |$\quad$| Remable window |
| :--- | :--- |


| Emergency stop button | Mounted on surface mounting <br> enclosure MZ521N | 1 | MZ530N |
| :--- | :--- | :--- | :--- |
| IP65 |  |  |  |

## Earth Fault Relays

Supply
Contactor/trip


HR400


HR420

| Designation | Characteristics | Width in 17.5 mm | Pack qty. | Cat Ref. |
| :---: | :---: | :---: | :---: | :---: |
| Earth fault relay <br> C/O contact <br> 6A~AC1 | Instant trip, fixed sensitivity $1 \Delta \mathrm{n}=30 \mathrm{~mA}$ | 2 | 1 | HR400 |
|  | 300 mA | 2 | 1 | HR402 |
| Earth fault relay <br> C/O contact <br> 6A~ AC1 <br> Adjustable sensitivity $\begin{aligned} & I \Delta n=30,100,300 \mathrm{~mA} \\ & 1 \& 3 A \end{aligned}$ | Instant trip or time delay $0.13-0.3-1 \& 3 \mathrm{sec}$ | 2 3 | 1 | HR403 HR410 |
| Earth fault relay <br> C/O contact <br> 6A~ AC1 <br> Positive safety <br> C/O contact | Standard version | 3 | 1 | HR411 |
| 6A~ AC1 <br> Adjustable <br> sensitivity $\mathrm{I} \Delta \mathrm{n}=30,100,300 \mathrm{~mA}$ $1 \& 3 A$ <br> Instant or time delayed $0.13-0.3-1 \& 3 \mathrm{sec}$ | Version with LED optical scale | 3 | 1 | HR420 |
|  | Version with LED optical scale and remote test | 5 | 1 | HR425 |

\(\left.\begin{array}{llll}\hline Earth leakage relay with integral \& 4 \& 1 \& HR440 <br>

torroid adjustable sensitivity\end{array}\right]\)| as above instant or time delayed | 6 | 1 |
| :--- | :--- | :--- | HR441

## Earth Fault Relay

- Torroids



HR822

## Surge Protection Devices <br> (SPD)



|  | Designation | Characteristics | Width in II 17.5 mm | Pack qty. | Cat Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Un: } 230 / 400 \mathrm{~V} \\ & 50 / 60 \mathrm{~Hz} \end{aligned}$ | Single pole Up: 1.2kV at In | 1 | 1 | SPN140D |
|  | $\begin{aligned} & \text { Un: } 230 / 400 \mathrm{~V} \\ & 50 / 60 \mathrm{~Hz} \end{aligned}$ | 2 poles, $1 \varnothing+\mathrm{N}$ with reserve indicator and auxiliary contacts Up: 1.0kV at In | 2 | 1 | SPN215R |
| $10$ | $\begin{aligned} & \text { Un: } 230 / 400 \mathrm{~V} \\ & 50 / 60 \mathrm{~Hz} \end{aligned}$ | 2 poles $1 \varnothing+\mathrm{N}$ Up: 1.0kV at In | 2 | 1 | SPN215D |
| SPN215D |  |  |  |  |  |
|  | $\begin{aligned} & \text { Un: } 230 / 400 \mathrm{~V} \\ & 50 / 60 \mathrm{~Hz} \end{aligned}$ | 4 pole $3 \varnothing+N$ with reserve indicator and auxiliary contacts Up: 1.2 kV at In | 4 | 1 | SPN415R |
|  | $\begin{aligned} & \text { Un: } 230 / 400 \mathrm{~V} \\ & 50 / 60 \mathrm{~Hz} \end{aligned}$ | 4 poles $3 \varnothing+\mathrm{N}$ Up: 1.0 kV at In | 4 | 1 | SPN415D |

## Surge Protection Devices <br> (SPD)



## 125A Frame MCCBs




HD105


HD149U

| Designation | Current rating (A) | Poles | $\begin{aligned} & \text { Icu } \\ & \text { kA } \end{aligned}$ | Ics <br> \% Icu | Pack qty | Cat Ref. 16KA | Cat Ref. $25 K A$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MCCB | 16 | 1 | 16 | 100 | 1 | HD101 | HH101 |
| MCCB | 20 | 1 | 16 | 100 | 1 | HD102 | HH102 |
| MCCB | 25 | 1 | 16 | 100 | 1 | HD103 | HH103 |
| MCCB | 32 | 1 | 16 | 100 | 1 | HD104 | HH104 |
| MCCB | 40 | 1 | 16 | 100 | 1 | HD105 | HH105 |
| MCCB | 50 | 1 | 16 | 100 | 1 | HD106 | HH106 |
| MCCB | 63 | 1 | 16 | 100 | 1 | HD107 | HH107 |
| MCCB | 80 | 1 | 16 | 100 | 1 | HD108 | HH108 |
| MCCB | 100 | 1 | 16 | 100 | 1 | HD109 | HH109 |
| МССВ | 125 | 1 | 16 | 100 | 1 | HD110 | HH110 |
| MCCB | 20-25 | 3 | 16 | 100 | 1 | HD143U | HH143U |
| MCCB | 32-40 | 3 | 16 | 100 | 1 | HD145U | HH145U |
| MCCB | 50-63 | 3 | 16 | 100 | 1 | HD147U | HH147U |
| MCCB | 63-80 | 3 | 16 | 100 | 1 | HD148U | HH148U |
| MCCB | 80-100 | 3 | 16 | 100 | 1 | HD149U | HH149U |
| MCCB | 100-125 | 3 | 16 | 100 | 1 | HD150U | HH150U |
| MCCB | 50-63 | 4 | 16 | 100 | 1 | HD167U |  |
| MCCB | 80-100 | 4 | 16 | 100 | 1 | HD169U |  |
| MCCB | 100-125 | 4 | 16 | 100 | 1 | HD170U |  |
| Non automatic | 125 | 3 |  |  | 1 | HC101 |  |
| Non automatic | 125 | 4 |  |  | 1 | HC102 |  |

## 125A frame MCCBs - <br> Accessories and Auxiliaries

| Earth fault blocks (4P only) | Internal auxiliaries | Auxiliary contact - allows remote |
| :--- | :--- | :--- |
| Mounting - right side | Shunt trip - for remote tripping of |  |
| indication of the MCCB |  |  |



HB112


HX122


HX131


HY122
Designation Pack Cat Ref.
qty

| Add-on earth fault block | 1 | HB112 |
| :--- | :--- | :--- |

Sensitivity - adjustable
$0.03,0.1,0.3,1,3,10 \mathrm{~A}$

Time delay settings
instantaneous
$0.06,0.15,0.3,0.5$, 1 s

|  | Coil rating <br> Designation | Power <br> consumption (VA) | Operating <br> voltage (Un) | Pack <br> qty | Cat Ref. |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Shunt trip | $12-60 \mathrm{~V} \mathrm{ac/dc}$ |  |  |  | HX101E |
|  | $110-240 \mathrm{~V} \mathrm{ac/dc}$ | 300 | $>75 \%$ | 1 | HX104E |
|  | $380-415 \mathrm{~V}$ ac | 300 | $>75 \%$ | 1 | HX105E |
| Under voltage release | $208-240 \mathrm{~V} \mathrm{ac}$ |  | $\leq 70 \%$ | 1 | HX114E |
|  | $380-500 \mathrm{~V}$ ac |  | $\leq 70 \%$ | 1 | HX115E |

Designation
Contact
rat. 400VAC
Contact
rat. 230VAC

Contact Pack
Cat Ref.
rat. 400VAC rat. 230VAC rat.110VAC qty

| Auxiliary contacts |  |  |  |  | HX122 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Auxiliary $2 \mathrm{~N} / \mathrm{O}$ | 1.5 A | 3 A | 4 A | 1 | HX |
| Auxiliary and alarm C/O | 1.5 A | 3 A | 4 A | 1 | HX123 |


| Designation | Type | Shaft <br> length $m m$ | Padlockable Pack <br> off <br> qty | Cat Ref. |
| :--- | :--- | :--- | :--- | :--- | :--- |

## 250A Frame MCCBs

|  | Description <br> The Hager range of MCCBs offer panelbuilders and OEM's, a wide choice of options. The 250A frame is available with a breaking capacity up to 40kA | Technical data <br> Standards - BS EN 60947-2 <br> Current rating - 160, 250A <br> Voltage - 230/400VAC <br> Short circuit capacity - <br> $3 \& 4 \mathrm{P}$ Icu $=\mathrm{Ics}=40 \mathrm{KA}$ |  |  | Thermal adjustment $3 \& 4 \mathrm{P}-0.8-1 \mathrm{x} \ln$ <br> magnetic adjustment-3 \& 4P 5-10x In <br> Cable capacity $-120 \mathrm{~mm}^{2}$, max bar width $=20 \mathrm{~mm}^{2}$ $\square$ For technical details see page 3.40-3.44 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Designation | Current rating (A) | Poles | $\begin{aligned} & \text { Icu } \\ & \text { kA } \end{aligned}$ | Ics <br> \%lcu | Pack qty | Cat Ref. |
|  | MCCB | 80 | 3 | 40 | 100 | 1 | HN251 |
|  | MCCB | 100 | 3 | 40 | 100 | 1 | HN252 |
|  | MCCB | 125 | 3 | 40 | 100 | 1 | HN253 |
|  | MCCB | 160 | 3 | 40 | 100 | 1 | HN254 |
|  | MCCB | 200 | 3 | 40 | 100 | 1 | HN203 |
|  | MCCB | 250 | 3 | 40 | 100 | 1 | HN204 |
| HH253 |  |  |  |  |  |  |  |
|  | MCCB | 160 | 4 | 40 | 100 | 1 | HN264 |
|  | MCCB | 200 | 4 | 40 | 100 | 1 | HN213 |
|  | MCCB | 250 | 4 | 40 | 100 | 1 | HN214 |
|  | Non automatic | 250 | 3 |  |  | 1 | HC203 |
|  | Non automatic | 250 | 4 |  |  | 1 | HC204 |

## 250A Frame MCCBs -

Accessories and Auxiliaries

| Earth fault blocks (4P only) | Internal Auxiliaries <br> Mounting - underneath | Shunt trip - for remote tripping of <br> the MCCB, operates when coil is |
| :--- | :--- | :--- | | Auxiliary contact - allows remote |
| :--- |
| indication of the MCCB contacts |
| Alarm contact - remotely |
| indicates the tripped status of |



Designation $\quad$| Pack |
| :--- |
| qty |$\quad$ Cat Ref.

| Add-on Earth Fault Block | 1 | HB211 |
| :--- | :--- | :--- |

Senstivity - adjustable
$0.03,0.1,0.3,1,3,10 \mathrm{~A}$

Time delay settings
instantaneous
$0.06,0.15,0.3,0.5,1 \mathrm{~s}$

HX104E

| Designation | Coil rating <br> (V) | Power consumption (VA) | Operating voltage (Un) | Pack qty | Cat Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Shunt trip |  |  |  |  |  |
|  | $\begin{aligned} & \text { 12-60V } \\ & \text { AC/DC } \end{aligned}$ | 300 | > $75 \%$ | 1 | HX101E |
|  | $110-240 \mathrm{~V}$ <br> AC/DC | 300 | > $75 \%$ | 1 | HX104E |
|  | 380-415V AC | 300 | >75\% | 1 | HX105E |
| Under voltage release |  |  |  |  |  |
|  | 230 | 5 | <70\% | 1 | HX114E |
|  | 400 | 5 | ¢70\% | 1 | HX115E |


| Designation | Contact | Contact | Contact | Pack | Cat Ref. |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | rat. 400VAC | rat. 230VAC | 110 VAC | qty |  |

## Auxiliary contacts

| Auxiliary 2 N/O | 1.5 A | 3 A | 4 A | 1 | HX122 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Auxiliary and alarm C/O | 1.5 A | 3 A | 4 A | 1 | HX223E |


| Designation | Type | Shaft <br> length $m m$ | Padlockable Pack <br> off | qaty Ref. |
| :--- | :--- | :--- | :--- | :--- |


| Rotary handles |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | direct | - | yes | 1 | HX230 |
|  | indirect | 200 mm | yes | 1 | HX231 |


| Accessories |  |  |
| :--- | :--- | :--- | :--- |
| Terminal shield 3P | 2 | HY221 |
| Terminal shield 4P | 2 | HY222 |
| Padlock attachment - for standard toggle | 1 | HX239 |

## 400A Frame MCCBs

| Description | Technical data | Thermal adjustment | $\square$ For technical details |
| :--- | :--- | :--- | :--- |
| The Hager range of MCCBs offer | Complies with - BS EN 60947-2 | $3 \& 4 \mathrm{P}-0.8-1 \mathrm{x} \mathrm{In}$ | see page $3.40-3.44$ |
| panelbuilders and OEM's, a wide | Current rating $-250-400$ | magnetic adjustment $-3 \& 4 \mathrm{P}$ |  |
| choice of options. The 400A | Voltage $-230 / 400 \mathrm{VAC}$ | $5-10 \times \mathrm{In}$ |  |
| frame is available with a range of | Short circuit capacity | cable capacity $-240 \mathrm{~mm}^{2}$, max |  |
| auxiliaries or accessories. | Icu $=\mathrm{Ics}=45 \mathrm{KA}$ | bar width $=32 \mathrm{~mm}^{2}$ |  |


|  | Designation | Current rating (A) | Poles | $\begin{aligned} & \text { Icu } \\ & \text { kA } \end{aligned}$ | Ics <br> \% Icu | Pack qty | Cat Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 . g^{0} g^{\theta}$ | MCCB | 250 | 3 | 50 | 100 | 1 | HN301E |
| is | MCCB | 320 | 3 | 50 | 100 | 1 | HN302E |
|  | MCCB | 400 | 3 | 50 | 100 | 1 | HN303E |
|  | MCCB | 250 | 4 | 50 | 100 | 1 | HN321E |
|  | MCCB | 320 | 4 | 50 | 100 | 1 | HN322E |
| -2- | MCCB | 400 | 4 | 50 | 100 | 1 | HN323E |
|  | non auto | 400 | 3 |  |  | 1 | HC301E |
|  | non auto | 400 | 4 |  |  | 1 | HC302E |

HN303E

400A frame MCCBs -
Accessories and Auxiliaries

|  | Designation | Coil rating (V) | Power consumption (VA) | Operating voltage (Un) | Pack qty | Cat Ref. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| HX104E | Shunt trip |  |  |  |  |  |
|  |  | 12-60V | 300 | >75\% | 1 | HX101E |
|  |  | AC/DC |  |  |  |  |
|  |  | 110-240V | 300 | >75\% | 1 | HX104E |
|  |  | AC/DC |  |  |  |  |
|  |  | 380-415 AC | 300 | >75\% | 1 | HX105E |
|  | Under voltage release |  |  |  |  |  |
|  |  | 208-240V | 5 | s70\% | 1 | HX114E |
|  |  | 380-500V | 5 | s70\% | 1 | HX115E |
|  | Designation | Contact | Contact | Contact | Pack | Cat Ref. |
|  |  | rat. 400VAC | rat. 230VAC | 110VAC | qty |  |
|  | Auxiliary contacts |  |  |  |  |  |
|  | Auxiliary 2 N/O | 1.5A | 6A | 4A | 1 | HX122 |
|  | Auxiliary and alarm C/O | 1.5A | 3A | 4A | 1 | HX223E |
| HX722 |  |  |  |  |  |  |
|  | Designation | Type | Shaft length mm | Padlockable off | Pack qty | Cat Ref. |
|  | Rotary handles |  |  |  |  |  |
|  |  | Direct | - | yes | 1 | HX330E |
|  |  | Indirect | 200 mm | yes | 1 | HX331E |
|  | Accessories |  |  |  |  |  |
|  | 3 pole shroud |  |  |  | 2 | HY321E |
|  | 4 pole shroud |  |  |  | 2 | HY322E |
|  | Toggle locking kit |  |  |  | 1 | HX339E |
| 3.30 | Hager C | gue 2007 • Protec | Devices |  |  |  |


| Description <br> The Hager range of MCCBs offer panelbuilders and OEM's, a wide choice of options. The 630A frame is available with a range of auxiliaries or accessories | Technical data <br> Standards - BS EN 60947-2 and IEC947-2 <br> Current rating - 500-800 <br> Voltage - 3 \& 4P 400/415VAC <br> Short circuit capacity - <br> $3 \& 4 \mathrm{P} \mathrm{Icu}=\mathrm{Ics}=50 \mathrm{KA}$ | Thermal adjustment $3 \& 4 P-0.8-1 x \ln$ <br> magnetic adjustment-3 \& 4P 5-10x In <br> cable capacity $-2 \times 240 \mathrm{~mm}^{2}$, <br> max bar width $=50 \mathrm{~mm}^{2}$ |  |  | $\square$ For technical details see page 3.40-3.44 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Designation | Current rating (A) | Poles | $\begin{aligned} & \text { Icu } \\ & \text { kA } \end{aligned}$ | ICS <br> \% Icu | Pack qty | Cat Ref. |
| PMM- | MCCB | 500 | 3 | 50 | 100 | 1 | HN802 |
|  | MCCB | 630 | 3 | 50 | 100 | 1 | HN803 |
|  | MCCB | 800 | 3 | 50 | 100 | 1 | HN806 |
| 12 | MCCB | 500 | 4 | 50 | 100 | 1 | HN812 |
|  | MCCB | 630 | 4 | 50 | 100 | 1 | HN813 |
|  | MCCB | 800 | 4 | 50 | 100 | 1 | HN816 |
| $0^{\circ} 0^{\circ}$ | non auto | 630 | 3 |  |  | 1 | HC801 |
|  | non auto | 630 | 4 |  |  | 1 | HC802 |
| HN802 | non auto | 800 | 3 |  |  | 1 | HC803 |
|  | non auto | 800 | 4 |  |  | 1 | HC804 |

630A frame MCCBs -
Accessories and Auxiliaries


## Circuit Protection Principle

## Basic Principles

The proper selection of the correct circuit protective device requires an understanding of the potential hazards against which protection for safety is required. The Wiring Regulations identify several hazards:

- Electric shock
- Thermal effects
- Overcurrent
- Undervoltage
- Isolation

Electric shock - is divided into two parts

- Direct contact: contact with parts which result in an electric shock in normal service
- Indirect contact: contact with exposed conductive parts which result in an electric shock in case of a fault.

To protect against direct contact the Wiring Regulations
suggest the following basic measures should be taken:
(1) by insulation of live parts
(2) by enclosures or barriers
(3) by obstacles
(4) by placing out of reach

To protect against indirect contact the Wiring Regulations suggest the following basic measures should be taken:
(1) Earthed equipotential bonding and automatic disconnection of supply
(2) Use of class II equipment or equivalent insulation
(3) Non-conducting location
(4) Earth-free local equipotential bonding
(5) Electrical separation

Of these five measures, the first is by far the most commonly used -
(1) Earthed equipotential bonding and automatic disconnection of supply:

In each installation circuit protective conductors connect all exposed conductive parts of the installation to the main earthing terminal. Main equipotential bonding conductors are used to connect extraneous conductive parts of other incoming services and structural metalwork to the main earthing terminal. These extraneous conductive parts include the following:

- Main water pipes
- Gas installation pipes
- Other service pipes and ducting
- Risers of central heating and air conditioning systems
- Exposed metal parts of the building structure

This bonding creates a zone within which any voltages appearing between exposed conductive parts and extraneous conductive parts, are minimised; the earth fault loop impedance must have a value low enough to allow sufficient current to flow for the circuit protective device to operate rapidly to disconnect the supply; disconnection must be sufficiently fast so that voltages appearing on the bonded metalwork cannot persist long enough to cause danger; depending on the operating characteristics of the protective device and the earth impedance, such disconnection may be achieved either by overcurrent devices, Fuses, Miniature Circuit Breakers, (i.e. MCBs) or by Residual Current Devices, (i.e. RCCBs).

Thermal Effect - refers to heat generated by the electrical equipment in normal use and under fault conditions. The proper selection of equipment complying with the latest product standards is essential in providing protection against thermal effects.

Overcurrent - is defined as a current exceeding the rated value of the circuit components. It may be caused by the overloading of a healthy circuit or it may take the form of a short-circuit current, defined as an "overcurrent resulting from a fault of negligible impedance between live conductors having a difference in potential under normal operating conditions". Overcurrent protection may be provided by using fuses or circuit breakers singly or in combination.

Undervoltage - refers to the dangers that could be caused by the reduction or loss in voltage and the subsequent restoration, such as the unexpected re-starting of motors or the automatic closing of protective devices. The proper selection of control and protective devices must take the protection against undervoltage into consideration.

Isolation - every circuit shall be provided with means of isolation (except in certain cases) to prevent or remove hazards associated with the installation, equipment and machines. The new standards for circuit breakers and switch-fuses now take this into account.

## Protection against shock by indirect contact

Indirect contact - is the contact of persons or livestock with exposed conductive parts made live by a fault and which may result in electric shock. An example would be where the insulation of an electric heater has broken down resulting in a live conductor internally touching the casing. This could result in the heater casing being raised to a hazardous voltage level, causing electric shock to a person touching it.

Two important measures must be taken to prevent this hazard:

- The impedance of circuit conductors is kept to a minimum. The earth fault loop impedance $(\mathrm{Zs})$ is used as a measure of the circuit impedance under fault conditions.
- The overcurrent device protecting the circuit is selected to rapidly disconnect an earth fault.

The effect of these two measures is inter-related.

1. By ensuring that the circuit protective conductor is of a low impedance, the voltage to which the live casing is raised, under fault conditions, is kept to a minimum
2. The low impedance path provided by the circuit conductors and the circuit protective conductor will result in a high level of current in the event of an earth fault. This high fault current ensures that the overcurrent protective device will disconnect the fault in a short time, reducing the interval during which the casing of the faulty equipment is live.


Fig 2
Components of earth fault loop impedance $\left(Z_{s}\right)$ in a system. (Earth fault at load between conductor and casing).
$Z_{s}=Z_{e}+\left(R_{1}+R_{2}\right)$

## Earth fault loop impedance $\left(Z_{s}\right)$

To ensure the impedance of conductors in a circuit is sufficiently low the system designer has to establish the value of the earth fault loop impedance.
$Z_{s}$ is a measure of the earth fault current loop, comprising the phase conductor and the protective conductor. It comprises the complete loop including the winding of the transformer from which the circuit is supplied as defined by the following:
$Z_{e}$ is the part of the earth fault loop impedance external to the installation, its value can be measured or a nominal value can be obtained from the supply authority.

## Circuit Protection Principle

$\left(\mathbf{R}_{1}+\mathbf{R}_{2}\right)$ - Where R1 is the resistance of the phase
conductor within the installation and $R 2$ is the resistance of the circuit protective conductor. These two components constitute the loop impedance within the installation.
Therefore: $Z_{s}=Z_{e}+\left(R_{1}+R_{2}\right)$
Once the value of $Z s$ has been established a suitable overcurrent protective device has to be selected to ensure disconnection of an earth fault within the specified time. The times are:

- 5 seconds for fixed equipment.
- For portable equipment and for fixed equipment installed outside the equipotential bonding zone, the disconnection times are dependent on the nominal
voltage to earth, i.e. 220 to 277 volts $=0.4$ seconds.


## $Z_{\text {s }}$ by Calculation

To establish whether the relevant disconnection time can be achieved a simple calculation must be made, based on Ohm's law:

If (fault current) $=\frac{\text { Uoc (open circuit voltage) }}{\text { Zs (earth fault loop) }}$

* voltage between phase and earth (240V)

The fault current (If) must be high enough to cause the circuit protective device to trip in the specified time. This can be established by consulting the time/current characteristic for the protective device. If the maximum trip time for the fault current calculated is less than or equal to the relevant value ( 5 s for fixed equipment; 0.4 s for portable equipment) then compliance is achieved. It is important that when consulting the characteristic curve the worst case is used, i.e. the maximum tripping time including any tolerance. An example is shown in Figs 1 and 2.

## $Z_{s}$ by tables

The above procedure can be used for any type of protective device providing a time/current characteristic curve is available. Frequently, however, a much simpler method is available using tables listing maximum Zs values which have been interpreted from the characteristic curves for the relevant devices. Providing the system Zs is equal to or less than the value given in the table, compliance is achieved. Tables for a number of 'standard' devices (certain fuses and MCBs) are given in the Wiring Regulations.

## $Z_{\mathrm{s}}$ too high

If the system Zs value is too high to achieve rapid enough disconnection with the overcurrent protective devices available then it is necessary to use one of the two following methods:

- Fit a cable with a larger cross-section and consequently a lower impedance. This may be a very expensive solution especially when the installation is complete before the problem is discovered.
- Use a Hager residual current device (RCCB). Subject to certain conditions being met this provides a simple and economical solution. Example



## Fig 2

Fig 2 shows a fixed circuit with an earth loop impedance $Z_{s}$ of 0.7 ohms protected with an MTN132. The fault current $\left(I_{f}\right)$ will therefore be $U_{o} / Z_{s}=240 / 0.7=343 \mathrm{~A}$

By referring to the characteristic for MTN132 (see Fig 3) it can be seen that the breaker will disconnect in 0.02 seconds for this current. The breaker therefore easily satisfies the requirement for disconnection in 5 seconds.

If the circuit $Z_{s}$ was 2.0 ohms then the fault current would be: $240 / 2=120 \mathrm{~A}$ and the disconnection time would be 10 seconds, in which case compliance would not be achieved.


Fig 3

## Protection against overcurrent

Overcurrent - "A current exceeding the rated value. For conductors the rated value is the current-carrying capacity"

Overload Current - "An overcurrent occurring in a circuit which is electrically sound"

Short-Circuit Current - "An overcurrent resulting from a fault of negligible impedance between live conductors having a difference in potential under normal operating conditions."

## Protection against Overload Current

For the protection against overload current, protective devices must be provided in the circuit to break any overload current flowing in the circuit conductors before it can cause a temperature rise which would be detrimental to insulation, joints, terminations or the surroundings of the conductors.

In order to achieve this protection the nominal current of the protective device $I_{n}$ should be not less than the design current of the circuit lb and that $\mathrm{I}_{\mathrm{n}}$ should not exceed the current-carrying capacity of the conductors $I_{z}$, and that the current causing effective operation of the protective device $I_{2}$ does not exceed 1.45 times the currentcarrying capacity of the conductor $I_{z}$, expressed as
$I_{b} \leq I_{n} \leq I_{z}$
$\mathrm{I}_{2} \leq 1.45 \mathrm{I}_{\mathrm{z}}$

## Protection against Short-Circuit Current

Protective devices must be provided to break any short-circuit current before it can cause danger due to thermal and mechanical (electro-dynamic) effects produced in the conductors and connections. The breaking capacity of the protective device shall not be less than the prospective short-circuit current at the point at which the device is installed. However a lower breaking capacity is permitted provided that a properly co-ordinated back-up device having the necessary breaking capacity is installed on the supply side (see page 3.43).

## Positioning of Overcurrent Devices

Devices for the protection against overload and short-circuit must be placed at the point where a reduction occurs in the current-carrying capacity of the conductors. This reduction could be caused by a change in the environmental conditions as well as the more obvious change in the cross-sectional area of the cable.

There are of course exceptions to this general rule which relate to a very few special applications. These are set out in detail in the Wiring Regulations.

## Circuit Breakers

Both of the new British Standards covering Low Voltage Circuit Breakers provide the user with a better assurance of quality and performance by taking into account the actual operating conditions of the breaker. New definitions and symbols have been introduced which should be committed to memory. Some of those most frequently used are:
$U_{e}$ : Rated service voltage
$U_{i}$ : Rated insulation voltage (> Uemax)
$\mathrm{U}_{\mathrm{imp}}$ : Rated impulse withstand
$I_{c m}$ : Rated short circuit making capacity
$\mathrm{I}_{\mathrm{cn}}^{\mathrm{cm}}$ : Rated short circuit capacity
$I_{c s}$ : Rated service short circuit breaking capacity
$I_{c u}$ : Rated ultimate short circuit breaking capacity
$I_{\Delta n}$ : Rated residual operating current (often called residual sensitivity)
$I_{n} \quad:$ Rated current = maximum value of current used for the temperature rise test
$\Delta_{t}$ : trip delay of residual current devices
In addition BS EN 60898 sets out to provide a greater degree of safety to the uninstructed users of circuit breakers. It is interesting to note that the description "miniature circuit breaker" or MCB is not used at all in this standard, but no doubt both manufacturers and users will continue to call circuit breakers complying with BS EN 60898 miniature circuit breakers or MCBs for some time to come.

The scope of this standard is limited to ac air break circuit breakers for operation at 50 Hz or 60 Hz , having a rated current not exceeding 125 A and a rated short-circuit capacity not exceeding 25kA.

A rated service short-circuit breaking capacity Ics is also included which is equal to the rated short-circuit capacity Icn for short-circuit capacity values up to and including 6kA, and 50\% of Icn above 6kA with a minimum value of 7.5 kA . As the circuit- breakers covered by this standard are intended for household and similar uses, Ics is of academic interest only. The rated short-circuit capacity of a MCB (Icn) is the alternating component of the prospective current expressed by its r.m.s. value, which the MCB is designed to make, carry for its opening time and to break under specified conditions. Icn is shown on the MCB label in a rectangular box without the suffix ' $A$ ' and is the value which is used for application purposes. Icn (of the MCB) should be equal to or greater than the prospective short-circuit current at the point of application.

You will see from the curves that the inverse time / current characteristic which provides overload protection is the same on all three. This is because the British Standard requires the breaker to carry 1.13 times the rated current without tripping for at least one hour and when the test current is increased to 1.45 times the rated current, it must trip within one hour, and again from cold if the current is increased to 2.55 times the rated current the breaker must trip between 1 and 120 seconds. The inverse time delay characteristic of all MCBs claiming compliance with BS EN 60898 must operate within these limits.

The difference between the three types of characteristic curves designated ' $B$ ', 'C' and 'D' concerns only the magnetic instantaneous trip which provides short-circuit protection.

- For type ' $B$ ' the breaker must trip between the limits of 3 to 5 times rated current
- For type 'C" the breaker must trip between the limits of 5 to 10 times rated current, and
- For type 'D' the breaker must trip between the limits of 10 to 20 times rated current.

Often manufacturers publish their MCB tripping characteristics showing the limits set by the standard and guarantee that any breaker that you purchase will operate within these limits. So great care should be taken when working with characteristic curves showing lower and higher limits - on no account should you take a mean point for application design purposes.

For cable protection applications you should take the maximum tripping time and some manufacturers publish single line characteristic curves which show the maximum tripping time. If the design problem is nuisance tripping then the minimum tripping time should be used and for desk top co-ordination studies, both lower and upper limits have to be taken into account.

## Energy limiting

Energy is measured in Joules. *James Prescott Joule proved that thermal energy was produced when an electric current flowed through a resistance for a certain time, giving us the formula :-

Joules $=12 \times R \times t$ or because we know that watts $=I 2 R$
Joules $=$ watts $\times$ seconds
Therefore we can say that :-
One Joule = one watt second
or energy = watts $x$ seconds $=12 R \mathrm{t}$
If the resistance $(\mathrm{R})$ remains constant or is very small compared with the current (I) as in the case of short-circuit current, then energy becomes proportional to 12 t . Which is why the energy let-through of a protective device is expressed in ampere squared seconds and referred to as I 2 t

12 t (Joule Integral) is the integral of the square of the current over a given time interval ( $\mathrm{t} 0, \mathrm{t} 1$ )

The 12 t characteristic of a circuit breaker is shown as a curve giving the maximum values of I 2 t as a function of the prospective current.

Manufacturers are required by the British Standard to produce the I 2 t characteristic of their circuit breakers.
See page 3.39.

The energy limiting characteristics of modern MCBs greatly reduce the damage that might otherwise be caused by short-circuits. They protect the cable insulation and reduce the risk of fire and other damage. Knowledge of the energy limiting characteristic of a circuit breaker also helps the circuit designer calculate discrimination with other protective devices in the same circuit.

Because of the importance of the energy limiting characteristic the British Standard for circuit breakers for household and similar installations suggests three energy limiting classes based on the permissible I2t (let-through) values for circuit breakers up to 32A; class 3 having the best energy limiting performance.

All Hager MCBs exceed the requirements for energy let-through set by the British Standard for energy limiting class 3.

## Circuit Breakers

| Electrical characteristics | References |  |  | NLN | NTN | NBN |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Table 11

* Din rail mount only, not for use in fixed busbar distribution boards.


## Power loss

The power loss of MCB's is closely controlled by the standards and is calculated on the basis of the voltage drop across the main terminals measured at rated current. The power loss of Hager circuit breakers is very much lower than that required by the British Standard, so in consequences run cooler and are less affected when mounted together.

The table below gives the watts loss per pole at rated current.

| MCB rated current (A) | 0.5 | 1 | 2 | 3 | 4 | 6 | 10 | 16 | 20 | 25 | 32 | 40 | 50 | 63 | 80 | 100 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Watts loss per pole (W) | 1.3 | 1.5 | 1.7 | 2.1 | 2.4 | 2.7 | 1.8 | 2.6 | 2.8 | 3.3 | 3.9 | 4.3 | 4.8 | 5.2 | 8 | 10 |

Table 12

## For use with DC

Because of their quick make and break design and excellent arc quenching capabilities Hager circuit breakers are suitable for DC applications.

The following parameters must be considered.
1 System voltage:
Determined by the number of poles connected in series
(See table 13)

2 Short circuit current:
(See table 14)
3 Tripping characteristics:

- The thermal trip remains unchanged
- The magnetic trip will become less sensitive requiring derating by $\sqrt{ } 2$ the ac value. (See table 14)

| No. of poles | 1 pole |  | 2 poles in series |  |
| :--- | :--- | :--- | :--- | :--- |
| Range | max <br> voltage | breaking <br> capacity <br> L/R=15 | max <br> voltage | breaking <br> capacity <br> L/R=15ms |
| MTN | 60 V | 6 kA | 125 V | 6 kA |
| NBN NCN NDN | 60 V | 10 kA | 125 V | 10 kA |

Table 13

| Characteristic curve | B |  | C |  | D |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Magnetic trip | 50 Hz | dc | 50 Hz | dc | 50 Hz | dc |
| Irm1 | 31 n | 4.5 ln | 5 ln | 7.5 ln | 101n | 15In |
| Irm2 | 5 ln | 7.5 ln | 101n | 15In | 20 In | 301n |

## Circuit Breakers

Note: The circuit breaker can have the linelload connected to either the top or bottom terminals

## Temperature Derating

MCBs are designed and calibrated to carry their rated current and to operate within their designated thermal time/current zone at $30^{\circ} \mathrm{C}$. Testing is carried out with the breaker mounted singly in a vertical plane in a controlled environment. Therefore if the circuit breaker is required to operate in conditions which differ from the reference conditions, certain factors have to be applied to the standard data. For instance if the circuit breaker is required to operate in a higher ambient temperature than $30^{\circ} \mathrm{C}$ it will require progressively less current to trip within the designated time/current zone.

## Correction Factor

The breaker is calibrated at a temperature of $30^{\circ} \mathrm{C}$.

| Temperature Correction |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In (A) | $30^{\circ} \mathrm{C}$ | $35^{\circ} \mathrm{C}$ | $40^{\circ} \mathrm{C}$ | $45^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $55^{\circ} \mathrm{C}$ | $60^{\circ} \mathrm{C}$ |
| 0.5 | 0.5 | 0.47 | 0.45 | 0.4 | 0.38 | - | - |
| 1 | 1 | 0.95 | 0.9 | 0.8 | 0.7 | 0.6 | 0.5 |
| 2 | 2 | 1.9 | 1.7 | 1.6 | 1.5 | 1.4 | 1.3 |
| 3 | 3 | 2.8 | 2.5 | 2.4 | 2.3 | 2.1 | 1.9 |
| 4 | 4 | 3.7 | 3.5 | 3.3 | 3 | 2.8 | 2.5 |
| 6 | 6 | 5.6 | 5.3 | 5 | 4.6 | 4.2 | 3.8 |
| 10 | 10 | 9.4 | 8.8 | 8 | 7.5 | 7 | 6.4 |
| 16 | 16 | 15 | 14 | 13 | 12 | 11 | 10 |
| 20 | 20 | 18.5 | 17.5 | 16.5 | 15 | 14 | 13 |
| 25 | 25 | 23.5 | 22 | 20.5 | 19 | 17.5 | 16 |
| 32 | 32 | 30 | 28 | 26 | 24 | 22 | 20 |
| 40 | 40 | 37.5 | 35 | 33 | 30 | 28 | 25 |
| 50 | 50 | 47 | 44 | 41 | 38 | 35 | 32 |
| 63 | 63 | 59 | 55 | 51 | 48 | 44 | 40 |
| 80 | 80 | 76 | 72 | 68 | 64 | 60 | 56 |
| 100 | 100 | 95 | 90 | 85 | 80 | 75 | 70 |

## Grouping factors

Consideration should also be given to the proximity heating effect of the breakers themselves when fully loaded and mounted together in groups. There is a certain amount of watts loss from each breaker depending on the trip rating which may well elevate the ambient air temperature of the breaker above the ambient air temperature of the enclosure.

Grouping factor (rated current reduce by factor K)

| no. of units $n$ | $K$ |
| :--- | :--- |
| $n=1$ | 1 |
| $2 \leq n<4$ | 0.95 |
| $4 \leq n<6$ | 0.9 |
| $6 \leq n$ | 0.85 |
| Table 16 |  |

## Example

Five circuit breakers are to be installed inside an enclosure in a switchroom which has an average ambient air temperature of $35^{\circ} \mathrm{C}$. Each circuit breaker will be required to supply a continuous current of 20A.

From Table 15 we would select a circuit breaker which has a rated current of 25 A at $30^{\circ} \mathrm{C}$ and 23.5 A at $35^{\circ} \mathrm{C}$. This takes care of the switchroom ambient air temperature of $35^{\circ} \mathrm{C}$, but we also have to take into account the grouping factor of five continuously loaded breakers mounted together in one enclosure. Table 16 gives us a grouping factor K of 0.9 . We then apply this grouping factor to the rated current at $35^{\circ} \mathrm{C}$ which gives us a circuit breaker rated current of $23.5 \times 0.9=21.15 \mathrm{~A}$ in the specified conditions.

## Frequency

Thermal - unchanged
Magnetic - value multiplied by coefficient K

| $\mathrm{F}(\mathrm{Hz})$ | $17 \mathrm{~Hz}-60 \mathrm{~Hz}$ | 100 Hz | 200 Hz | 400 Hz |
| :--- | :--- | :--- | :--- | :--- |
| K | 1 | 1.1 | 1.2 | 1.5 |

Table 17

```
'B' curve (BS EN 60-898)
MCBs: MTN rated 6-63A
        NBN rated 6-63A
```



Fig 6

| 'C' curve (BS EN 60-898) | 'D' curve (BS EN 60-898) |  |
| :--- | :--- | :--- |
| MCBs: | NCN rated 0.5-63A | MCBs: |
|  | NDN rated 6-63A |  |
|  | MLN rated $2-32$ A |  |
|  | HMD rated 80-125A |  |

NMF rated $80-100 \mathrm{~A}$


## Circuit Breakers

## Current limiting at 400V

## MTN NBN NCN NDN



Fig 7

HMF, HMC, HMD 80-125A


## Circuit Breakers \& RCCB Auxiliaries

## Functions

Tripping and indication auxiliary contacts are common to the range of multi-pole 10kA MCBs, and RCCBs. They should be mounted on the left hand side of the device.

## Auxiliary contact MZ201 (fig 9)

Allows remote indication of the status of the device contacts to which it is associated.

## Auxiliary contact and alarm contact MZ202

This accessory has two separate functions.
Like the MZ201 auxiliary contact, however the alarm contact will provide indication if the breaker trips under fault conditions.

## MZ203 shunt trip*

Allows tripping of the device by feeding the coil. The contacts also allow for remote indication of operation.

MZ206 under voltage release* (fig 10)
Allows the MCB to trip when the voltage drops or by pressing a remote off switch (ie emergency stop).

* Indication that the product has tripped due to the voltage release is provided by a flag on the product.


## Wiring diagram

MZ201 auxiliary contact and alarm contact


Fig 9

| Electrical characteristics |  |  |  |
| :---: | :---: | :---: | :---: |
|  | MZ201/MZ202 | MZ203 | MZ206 |
|  | $\begin{aligned} & 1 \times \mathrm{O} 1 \times \mathrm{C} \\ & \text { contact } \\ & 230 \mathrm{~V} \sim 6 \mathrm{~A} \\ & \mathrm{AC}-1 \end{aligned}$ |  |  |
| $\xrightarrow{\square}$ |  | $\begin{aligned} & 230-415 \sim \\ & 110-130 \ldots \end{aligned}$ | $\begin{aligned} & 230 \mathrm{~V} \sim \\ & 50 \mathrm{~Hz} \end{aligned}$ |

Table 18

## MZ206 under voltage release



Fig 10

## Electrical connection

By terminal fitted with fixed clamp screws wiring capacity.
Flexible : $2 \times 1.5 \mathrm{~mm}^{2}$
Rigid: $2 \times 1.5 \mathrm{~mm}^{2}$

MZ203
Power - 8VA
tolerance : -15\% of Un
MZ206
Latching voltage is between 35 and $70 \%$ of Un 230 V .
Coil consumption 3VA

## Grouping / Combination of Several Auxiliaries

On 2, 3 and 4 pole MCBs it is possible to associate 3 auxiliaries 2 indication auxiliaries and 1 release auxiliary. In this case, it is important to first fix the indication auxiliary (MZ201 and MZ202) and then the release auxiliary (MZ203 and MZ206)


Fig 11


MZ203 to MZ206

Fig 12

## Transformer Protection

When a transformer is switched on, a high inrush current occurs in the primary circuit of the transformer irrespective of the load on the secondary side. Correct selection of the primary circuit protective device will avoid the risk of nuisance tripping due to this inrush current. Tables 19 \& 20 show the recommended MCB's for the protection of single phase (230V) and three phase (400V) transformers.

## Single Phase 230V

| Transformer | Primary | Recommended MCB |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Rating (VA) | Current (A) | NBN | NCN | NDN |
| 50 | 0.22 | - | 1 | 6 |
| 100 | 0.43 | - | 2 | 6 |
| 200 | 0.87 | - | 3 | 6 |
| 250 | 1.09 | 6 | 4 | 6 |
| 300 | 1.30 | 10 | 4 | 6 |
| 400 | 1.74 | 10 | 6 | 6 |
| 500 | 2.17 | 16 | 10 | 6 |
| 750 | 3.26 | 16 | 10 | 6 |
| 1000 | 4.35 | 25 | 16 | 10 |
| 2500 | 10.87 | 63 | 40 | 20 |
| 5000 | 21.74 | - | 63 | 32 |
| 7500 | 32.60 | - | - | 50 |
| 10000 | 43.48 | - | - | 63 |
| Table 19 |  |  |  |  |

Table 19

## Three Phase 400V

| Transformer | Primary | Recommended MCB |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Rating (VA) | Current (A) | NBN | NCN | NDN |
| 500 | 0.72 | - | 3 | 6 |
| 750 | 1.08 | 6 | 4 | 6 |
| 1000 | 1.44 | 10 | 6 | 6 |
| 2000 | 2.88 | 16 | 10 | 6 |
| 3000 | 4.33 | 25 | 16 | 10 |
| 4000 | 5.77 | 32 | 20 | 10 |
| 5000 | 7.21 | 40 | 25 | 16 |
| 7500 | 10.82 | 63 | 32 | 20 |
| 10000 | 14.43 | - | 50 | 25 |
| 15000 | 21.64 | - | 63 | 32 |
| 20000 | 28.86 | - | - | 50 |
| 25000 | 36.07 | - | - | 63 |

Table 20

## Lighting circuit

Although the MCBs prime function is the protection of lighting circuits, they are often used as local control switches as well, conveniently switching on and off large groups of luminaries in shops and factories. The MCB is well able to perform this additional task safely and effectively. Hager MCBs have an electrical endurance of 20,000 on/off operations for rated trips up to and including 32A and 10,000 on/off operations for 40, 50 and 63A rated trips. Account must be taken of the effects of switching inductive loads.

For the protection of lighting circuits the designer must select the circuit breaker with the lowest instantaneous trip current compatible with the inrush currents likely to develop in the circuit.

High Frequency (HF) ballasts are often singled out for their high inrush currents but they do not differ widely from the conventional 50 Hz . The highest value is reached when the ballast is switched on at the moment the mains sine wave passes through zero. However, because the HF system is a "rapid start" system whereby all lamps start at the same time, the total inrush current of an HF system exceeds the usual values of a conventional 50 Hz system. Therefore where multiple ballasts are used in lighting schemes, the peak current increases proportionally.

Mains circuit impedance will reduce the peak current but will not affect the pulse time.

The problem facing the installation designer in selecting the correct circuit breaker is that the surge characteristic of HF ballasts vary from manufacturer to manufacturer. Some may be as low as 12A with a pulse time of 3 mS and some as high as 35 A with a pulse time of 1 mS . Therefore it is important to obtain the expected inrush current of the equipment from the manufacturer in order to find out how many HF ballasts can safely be supplied from one circuit breaker without the risk of nuisance tripping.

This information can then be divided into the minimum peak tripping current of the circuit breaker, shown in Table below

## Circuit

Breaker Circuit breaker rated current

| type | $6 A$ | $10 A$ | $16 A$ | $20 A$ | $25 A$ | $32 A$ | $40 A$ | $50 A$ | $63 A$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| B | 26 | 43 | 68 | 85 | 106 | 136 | 170 | 212 | 268 |
| C | 43 | 71 | 113 | 142 | 177 | 223 | 283 | 354 | 446 |
| D | 85 | 142 | 226 | 283 | 354 | 453 | 566 | 707 | 891 |
| Table 21 |  |  |  |  |  |  |  |  |  |

## Minimum peak tripping current

Example:
How many HF ballasts, each having an expected inrush of 20A can be supplied by a 16A type C circuit breaker? From Table 21, 16A type C we have a minimum peak tripping current of 113A.

Therefore $\frac{113=5}{20}$
i.e. 5 ballasts can be supplied by a 16A type $C$ circuit breaker.

## Moulded case circuit breakers

Moulded case circuit breakers have been developed for use in commercial and industrial installations and, as the name implies, the air-break circuit breaker mechanism is housed in a moulded case of non-conducting material which not only provides a frontal protection of at least IP30 but also provides full segregation of all live parts. The main features of a modern Moulded Case Circuit Breaker (MCCB) are:

1. High breaking capacity and low specific let-through energy, ensuring full operating safety under heavy fault conditions.
2. Simultaneous opening and closing of all main poles.
3. Trip free mechanism.
4. Positive contact indication whereby the toggle always indicates the exact position of the main contacts
5. Test button which allows periodic testing of the mechanical trips.

MCCBs are intended to be selected, installed and used by skilled or instructed people and as such should comply with and be tested to BS EN 60947-2.

This British Standard, unlike BS EN 60898 which covers circuit breakers for household and similar installations does not set out to standardise the circuit breakers time/current characteristics. It does however give two points at which the time/current characteristics should be verified. The circuit breaker should be able to carry 1.05 times the thermal trip setting current without tripping and when loaded to 1.3 times that current to trip in one hour or less and in two hours or less for rated current above 63A.
Ir = Thermal trip setting.
Ics = Rated service short circuit capacity.
Icu = Rated ultimate short circuit capacity.

## Category A MCCB Characteristc Curve



## Category B MCCB characteristic curve



## Short-time withstand current Icw

BS EN 60947-2 defines two categories of circuit breakers:

Category ' $A$ ' for which no short-circuit trip delay is provided. These are generally the smaller moulded case circuit breakers below 630A with time current characteristics as shown in Fig 12.Category ' $A$ ' breakers will trip instantaneously when the short-circuit current is greater than the magnetic trip setting of the circuit breaker.

Category ' $A$ ' circuit breakers are suitable for current discrimination but not for time discrimination.

Category ' $B$ ' for which, in order to achieve time discrimination, it is possible to delay tripping during short-circuit conditions with values lower than Icw (As shown in Fig 13). These are generally the larger moulded case circuit breakers and air circuit breakers with time current characteristics as shown in Table 23. For moulded case circuit breakers Icw is always lower than the ultimate breaking capacity Icu.

The British Standard gives minimum values of Icw and of the associated time delay. See Table 22

| Short time withstand required for Icw |  | Associated delay |
| :--- | :--- | :--- |
| $\mathrm{I}_{\mathrm{n}} \leq 2500 \mathrm{~A}$ | $\mathrm{I}_{\mathrm{n}}>2500 \mathrm{~A}$ | $\Delta \mathrm{t}(\mathrm{s})$ |
| $\mathrm{I}_{\mathrm{cw}} \geq 12 \ln (\min 5 \mathrm{kA})$ | $\mathrm{I}_{\mathrm{cw}} \geq 30 \mathrm{kA}$ | 0.05 minimum value |
|  |  | $0.1 \quad)$ |
|  |  | $0.25)$ preferred |
|  | $0.5 \quad$ ) values |  |
|  | $1 \quad)$ |  |

Table 22

| Frame <br> (A) | thermal <br> rating Ith | rated <br> voltage <br> Ue(V) | rated short <br> time withstand <br> Icw (A) | impulse <br> voltage <br> Uimp (kV) | insulation <br> voltage <br> Ui (V) | no mechanical <br> operations | no electrical <br> operations |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 125 | 125 | $230 / 415$ | $1.7^{*}$ | 6 | 500 | 6000 | 6000 |
| 250 | 250 | 415 | $3.0^{*}$ | 8 | 690 | 6000 | 6000 |
| 400 | 400 | 415 | $4.8^{\star}$ | 8 | 750 | 16000 | 16000 |
| 630 | 630 | 415 | $7.5^{\star}$ | 8 | 750 | 16000 | 16000 |
| 800 | 800 | 415 | $9.6^{\star}$ | 8 | 750 | 16000 | 16000 |

* half second rating

Table 23

# MCCB Breaking Capacity \& <br> Temperature Derating 

## Breaking Capacity

An attempt has been made to try and make the assigned shortcircuit breaking capacities of a circuit breaker more understandable to the specifier and of more practical use to the designer than the old P1 and P2 ratings. The British Standard still specifies two ratings
$I_{\mathrm{cu}}$ : Rated ultimate short-circuit breaking capacity
$I_{c s}$ : Rated service short-circuit breaking capacity.
Ultimate Short Circuit Breaking Capacity
Icu corresponds in practice to P1 in the former standard and is defined in the same way. This is now covered under test sequence 3 , which is:

- Verify the overcurrent releases at 2.Ir;
- Two successive breaks at Icu,
cycle 0-3 min-CO;
- Dielectric withstand at $2 \mathrm{Ue}(50 \mathrm{~Hz}, 1 \mathrm{~min})$;
- Verify the calibration of the over-current releases.
$I_{c u}$ Represents the maximum short-circuit current which the breaker can break and is to be compared with the prospective fault current at the point of installation:
$I_{c u}$ (Of the device) Must be equal to or greater than the prospective short-circuit at the point of installation.


## Service Short-circuit Breaking Capacity

Generally, when a short-circuit occurs (in itself a very rare occurrence) its value is much lower than its calculated value. Nonetheless, it is essential that these lower values of short- circuit are cleared effectively and safely, and that the supply is re-established as quickly as possible. It is for this reason that BS EN 60947-2 has introduced a new characteristic. $I_{\text {cs }}$ known as Service Breaking Capacity and generally expressed as a percentage of $\mathrm{I}_{\mathrm{cu}}$. The value can be chosen by the manufacturer from $25,50,75$ or $100 \%$.
$I_{\text {cu }}$ must be verified as described under test sequence 2 which is:

- Three successive breaks at Ics with
cycle 0-3 min - CO-3 min-CO;
- Dielectric withstand at $2 \mathrm{Ui}(50 \mathrm{~Hz}, 1 \mathrm{~min})$;
- Temperature rise at In;
- Verify the calibration of the over-current releases.

This establishes $I_{c s}$ as a performance characteristic which can be considered not simply as a breaking capacity (as was the case of P2) but as the ability of the circuit breaker to ensure normal service, even after having disconnected several short-circuits.

The percentage ratio of $\mathrm{I}_{\mathrm{cs}}$ to $\mathrm{I}_{\mathrm{cu}}$ is another important aspect for the designer to understand. Our wiring regulations, which are based on IEC 364, give no guidance at the moment on the use of performance characteristic Ics. To comply with these regulations it is only necessary for the ultimate breaking capacity of the protective device to be equal to or greater than prospective fault level: $I_{c u} \geq I_{c s}$.

The selection of the percentage ratio of $\mathrm{I}_{\mathrm{cs}}$ to $\mathrm{I}_{\mathrm{cu}}$ to achieve optimum continuity of service depends on the "probable short circuit level". Therefore Ics should be equal to or greater than the probable short circuit level. However for large air circuit breakers it is usual for $I_{c s}=I_{c u}$, i.e. $100 \%$ because these devices are usually installed as main incomers to large switchboards where their field of protection is often limited to the switchboard itself. In these conditions the probable $I_{c s}$ will be only slightly less in comparison with the $I_{c u}$.

While this holds true for large switchboards, designed for high prospective fault levels, it is possible to use lower rated circuit breakers as incomers on panelboards designed for a relatively low prospective fault level. This provided that the service performance level is equal to or greater than the prospective fault level.
For example, it is possible to install an H 630 moulded case circuit breaker as a main incomer on a switchboard supplied from a 400kVA transformer because the H630 Ics is greater than the PSCC.

However, for those circuit breakers which are usually installed as outgoers, protecting cables to sub-boards or other loads, a $50 \%$ ratio is adequate because studies have shown that when a short-circuit does occur it is nearly always single or two phase and located at the extremity of the protected cable, and is usually less than $25 \%$ of the prospective fault level at the origin of the system and, in almost all cases, not greater than $50 \%$. It is therefore a wise precaution, to prolong the working life of the installation, to choose a device having a service performance Ics equal to $50 \%$ Icu. It is advisable to base the Ics rating of a MCCB on the pscc at the extremity of the circuit that it is protecting.

## Temperature Derating

Hager MCCBs are designed and calibrated to carry their rated current and to operate within this designated thermal time/current zone at $40^{\circ} \mathrm{C}$. If the ambient temperature around the circuit breaker differs from $40^{\circ} \mathrm{C}$ then it requires more or less current to operate the thermal trip depending on the ambient temperature variation.

Table 24 shows the variation of the range of the thermal trip as a function of the ambient temperature. The instantaneous magnetic trip is not affected by variations in ambient temperature.

## Variation of Thermal Trip Range with Ambient Temperature

|  |  | $30^{\circ} \mathrm{C}$ |  | $40^{\circ} \mathrm{C}$ |  | $50^{\circ} \mathrm{C}$ |  | $60^{\circ} \mathrm{C}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Type | In | min | max | min | max | min | max | min | max |
| 125A | 16 | - | 16.0 | - | 16.0 | - | 15.4 | - | 14.0 |
|  | 20 | - | 20.0 | - | 20.0 | - | 19.2 | - | 18.0 |
|  | 25 | - | 25.0 | - | 25.0 | - | 24.0 | - | 25.5 |
|  | 32 | - | 32.0 | - | 32.0 | - | 30.7 | - | 28.8 |
|  | 40 | - | 40.0 | - | 40.0 | - | 38.4 | - | 36.0 |
|  | 50 | - | 50.0 | - | 50.0 | - | 48.0 | - | 45.0 |
|  | 63 | - | 63.0 | - | 63.0 | - | 60.5 | - | 56.7 |
|  | 80 | - | 80.0 | - | 80.0 | - | 76.8 | - | 72.0 |
|  | 100 | - | 100.0 | - | 100.0 | - | 96.0 | - | 90.0 |
|  | 125 | - | 125.0 | - | 125.0 | - | 120.0 | - | 112.5 |
| 250A | 160 | 128.0 | 160.0 | 128.0 | 160.0 | 122.9 | 153.6 | 115.2 | 144.0 |
|  | 200 | 160.0 | 200.0 | 160.0 | 200.0 | 153.6 | 192.0 | 144.0 | 180.0 |
|  | 250 | 200.0 | 250.0 | 200.0 | 250.0 | 192.0 | 240.0 | 180.0 | 225.0 |
| 400A | 320 | 256.0 | 320.0 | 256.0 | 320.0 | 245.8 | 307.2 | 230.4 | 288.0 |
|  | 400 | 320.0 | 400.0 | 320.0 | 400.0 | 307.2 | 384.0 | 288.0 | 360.0 |
| 630A | 500 | 400.0 | 500.0 | 400.0 | 500.0 | 384.0 | 480.0 | 360.0 | 450.0 |
|  | 630 | 504.0 | 630.0 | 504.0 | 630.0 | 483.8 | 604.8 | 453.6 | 567.0 |
| 800A | 800 | 640.0 | 800.0 | 640.0 | 800.0 | 614.4 | 768.0 | 576.0 | 720.0 |

Table 24

It is important for this application to select a device where
$I_{c s}$ performance is close to $I_{c u}$.

| Frame type |  | 125 | 125 | 250 | 400 | 630 | 800 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rated current at $40^{\circ} \mathrm{C}$ | Amps | 125 | 125 | 250 | 400 | 630 | 800 |
| No. of poles |  | 1 | 3-4 | 3-4 | 3-4 | 3-4 | 3-4 |
|  | height mm | 140 | 140 | 176 | 257 | 273 | 273* |
|  | width mm | 25 | 75/101 | 105/140 | 140/183 | 210/273 | 210/273* |
|  | depth mm | 74 | 74 | 91 | 103 | 103 | 103 |
| Rated voltage Ue | V a.c. ( $50-60 \mathrm{~Hz}$ ) | 500 | 500 | 690 | 690 | 750 | 750 |
|  | 230-240V a.c. | 16 | 25 | 85 | 85 | 85 | 65 |
|  | 400-415V a.c. |  | 16 | 40 | 45 | 50 | 50 |
|  | 690 V a.c. |  |  |  | 20 | 20 | 20 |
|  | 250V d.c. | 20 | 20 | 20 | 20 | 20 | 20 |
|  | 400V a.c. | 100\% | 100\% | 100\% | 100\% | 100\% | 50\% |
| Releases |  |  |  |  |  |  |  |
| Rated current (product range) |  | 16-125A | 16-125A | 160-250A | 320-400A | 500-630A | 800A |
| Adjustable thermal releases | In | Fixed | 0.8-1.0 | 0.8-1.0 | 0.8-1.0 | 0.8-1.0 | 0.8-1.0 |
| Adjustable magnetic releases | In | Fixed | Fixed | 5.0-10.0 | 5.0-10.0 | 5.0-10.0 | 2.0-8.0 |
| Selective category B type |  |  |  |  | available | available | available |
| MCCBs BS EN 60947-2 |  |  |  |  | on request | on request | on request |
| Moulded case switches |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Internal accessories |  |  |  |  |  |  |  |
| Shunt trip |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Under voltage releases |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Auxiliary contacts |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Alarm contacts |  |  | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ | $\checkmark$ |
| Table 25 <br> * excludes terminal extension <br> For other control voltages plea | ds consult us. |  |  |  |  |  |  |


| Frame type | Designation | $125$ <br> Cat Ref. |  | $250$ <br> Cat Ref. |  | $400$ <br> Cat Ref. |  | 630/800 <br> Cat Ref. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Control voltage |  | 230 V | 400 V | 230 V | 400 V | 230 V | 400 V | 230 V | 400 V |
|  | Shunt trip operating voltage $\mathrm{UF}=0.7 \text { to } 1.1 \mathrm{Un}$ | HX104E | HX105E | HX104E | HX105E | HX104E | HX105E | HX804 | HX805 |
|  | Under voltage release Release voltage UF $=0.35$ to $0.7 U n$ Maintaining voltage $U F \geq 0.85 U n$ | HX114E | HX115E | HX114E | HX115E | HX114E | HX115E | HX814 | HX815 |
|  | Auxiliary contacts (2 off) | HX122 | - | HX122 | - | HX122 | - | HX822 | - |
|  | Auxiliary and alarm | HX123 | - | HX223 | - | HX223E | - | HX823 | - |

[^1]

Fig 14

|  |  |  |  |  | Direct start |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :---: |
|  |  | Full load <br> speed <br> rev/min | Full load <br> current <br> A | Starting <br> current <br> x FLC | Starting <br> torque <br> x FLC |  |
|  |  | 2800 | 3.2 | 6.75 | 3 |  |
|  |  | 1400 | 3.5 | 5.5 | 2.5 |  |
| 1.5 | 2 | 900 | 3.8 | 4.5 | 2.2 |  |
|  |  | 700 | 4.3 | 4.0 | 2.0 |  |

Table 27


Fig 15

## Motor Power Circuit Protection

The selection of the circuit protective device for motor power supply circuits depends in the first instance on the relative physical position of the various circuit elements. The feeder circuit breaker in the switchboard, panelboard or distribution board, the starter with its contactor and thermal overload relay, with perhaps its own isolator or short-circuit protective device (SCPD) and of course the motor.

The feeder circuit breaker, which can be a perfectly standard thermal magnetic breaker, must protect the cable feeding the starter so the normal selection criteria apply. In addition, however, it must be able to withstand the inrush and starting currents of the motor without nuisance tripping. The inrush current, which should not be confused with the starting current, appears at the instant of switch on and could be as great as 10 times the full load current (FLC) of the motor, but with a relatively short pulse time of 20 to 30 milliseconds.

The starting current of a direct on line (DOL) start squirrel cage motor does vary with the designed speed of the motor - the higher the speed the higher the starting torque and the starting current as a ratio of the FLC. However the FLC is inversely proportional to the design speed of the motor. Table 27 shows typical performance data for average $1.5 \mathrm{kw} / 2 \mathrm{hp}$ three phase squirrel cage motors.

The run-up time can vary between one and fifteen seconds depending on the surge of the motor and the type of load the motor is driving.

Clearly then, to accurately select the correct circuit breaker for a motor power supply circuit it is essential to know the correct FLC, the starting current and the run-up time. This information is then plotted against the time/current characteristic curve of the type of circuit breaker (or fuse) selected.

## Example

Select an appropriate feeder circuit breaker to supply a 1.5 kw 3 phase motor DOL start. FLC 3.5A, starting current $5.5 \times$ FLC, run-up time 6 secs. The circuit breaker must be suitable for fitting into a 3 phase MCB Distribution Board.

Starting current: $\quad 3.5 \times 5.5=19.25 \mathrm{~A}$ for 6 secs
Inrush current: $\quad 3.5 \times 10=35 A$
Comparing the data against the time/current characteristics of a type C MCB, Fig 15, we see that at 6 secs the breaker will carry $2 \mathrm{x} \ln$ without tripping. Therefore a 10A MCB would carry 20A for 6 secs. The minimum instantaneous trip for this type C MCB would be 50A.

Therefore the closest protection for this motor feeder circuit would be a 3 Pole 10A type C MCB. A 10A type D could be used providing the 100A maximum instantaneous trip was not a problem. The inrush current would preclude the use of a 10A type B because the minimum instantaneous trip is only 30A. In this case use the next size up, i.e. 16A.

| Motor <br> rating | DOL starting <br> conditions | Assisted start <br> conditions |
| :--- | :--- | :--- |
| Up to 0.75 kW | $5 \times$ FLC for 6 secs | $2.5 \times$ FLC for 15 secs |
| 1.1 to 7.5 kW | $6 \times$ FLC for 10 secs | $2.5 \times$ FLC for 15 secs |
| 11 to 75 kW | $7 \times$ FLC for 10 secs | $2.5 \times$ FLC for 15 secs |
| 90 to 160 kW | $6 \times$ FLC for 15 secs | $2.5 \times$ FLC for 20 secs |
| Table 28 |  |  |

## 1 Phase 230V DOL Starting

|  |  |  | Recommended circuit breaker |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :---: |
| kW | hp | A | (A) <br> NBN | HN <br> NCN | NDN | Fuse(A) |  |
| 0.18 | 0.25 | 2.8 | 16 | 10 | 10 | 10 |  |
| 0.25 | 0.33 | 3.2 | 16 | 10 | 10 | 16 |  |
| 0.37 | 0.5 | 3.5 | 16 | 10 | 10 | 16 |  |
| 0.55 | 0.75 | 4.8 | 20 | 16 | 16 | 16 |  |
| 0.75 | 1.0 | 6.2 | 25 | 20 | 20 | 20 |  |
| 1.1 | 1.5 | 8.7 | 40 | 25 | 25 | 25 |  |
| 1.5 | 2.0 | 11.8 | 50 | 32 | 32 | 32 |  |
| 2.2 | 3.0 | 17.5 | - | 50 | 50 | 40 |  |
| 3.0 | 4.0 | 20 | - | 63 | 63 | 50 |  |
| 3.75 | 5.0 | 24 | - | - | - | 63 |  |
| 5.5 | 7.5 | 36 | - | - | - | 80 |  |
| 7.5 | 10 | 47 | - | - | - | 100 |  |
| Table 29 |  |  |  |  |  |  |  |

3 Phase 400V Assisted Starting Star-Delta

| kW | hp | $\begin{aligned} & \text { FLC } \\ & \text { A } \end{aligned}$ | Recommended circuit breaker |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \text { (A) } \\ & \text { NCN } \end{aligned}$ | (A) NDN | HRC <br> fuse (A) |
| 3 | 4 | 6.3 | 16 | 10 | 16 |
| 4 | 5.5 | 8.2 | 20 | 10 | 16 |
| 5.5 | 7.5 | 11.2 | 32 | 16 | 20 |
| 7.5 | 10 | 14.4 | 40 | 25 | 25 |
| 11 | 15 | 21 | 50 | 32 | 32 |
| 15 | 20 | 27 |  | 40 | 35 |
| 18.5 | 25 | 32 |  | 50 | 40 |
| 22 | 30 | 38 |  | 63 | 50 |
| 30 | 40 | 51 |  |  | 63 |
| 37 | 50 | 63 |  |  | 80 |
| 45 | 60 | 76 |  |  | 80 |
| 55 | 75 | 91 |  |  | 100 |
| 75 | 100 | 124 |  |  | 160 |
| 90 | 125 | 154 |  |  | 200 |
| 110 | 150 | 183 |  |  | 200 |
| 132 | 175 | 219 |  |  | 250 |
| 150 | 200 | 240 |  |  | 315 |
| 160 | 220 | 257 |  |  | 315 |

Table 30

## Prospective Fault Current

## Prospective Short Circuit Current (PSCC) <br> 

Fig 16
In order to select the correct device for the proper protection against short-circuit current the Wiring Regulations suggest that the prospective short-circuit current at every relevant point of the complete installation shall be determined by calculation or by measurement of the relevant impedances.

Of course this is only necessary if the prospective short- circuit current at the origin of the installation is greater than the breaking capacity of the smallest protective device.

All short-circuit current protective devices must have a breaking capacity equal to or greater than the prospective fault current at the point where they are to be installed
$\mathrm{I}_{\mathrm{cn}} \geq$ Prospective fault current
The relationship between prospective fault current and probable fault current is discussed later.

## Prospective Fault Current

The theoretical maximum fault condition at any point in a distribution system is termed the "prospective fault current". This is the rms value of the current that would flow on the occurrence of a solidly bolted direct fault at that point and pre-supposes that the voltage will remain constant and the ultimate supply source has limitless capacity. Therefore, the prospective fault current is limited by

- The impedance of the high voltage network feeding the supply transformer.
- The impedance of the supply transformer.
- The impedance of the distribution Network from the supply transformer to the point of fault.
In practice the voltage does drop and the fault does have impedance and moreover the protective devices have impedance. Therefore the prospective current is theoretical and cannot be exceeded.

The severity of the short-circuit fault is also controlled by the "Power Factor" which like the fault current is determined by the circuit conditions up to the point of fault. However, the short-circuit power factor is not to be confused with the load power factor which is determined by the characteristics of the load itself.

Power Factor is effectively a measure of stored energy in the system. Hence if the power factor is low, there is a considerable amount of stored energy to be dissipated during the fault clearance. Also there will be a degree of asymmetry of the current wave due to the presence of a dc component.

## Asymmetrical Short Circuit Current

When a short-circuit occurs in a circuit the resistance of which is negligible compared with the inductive reactance, the resulting short-circuit current has a dc component. This dc component has a maximum value when the short-circuit occurs at the instant at which the circuit voltage is zero. (see Fig 17). Since in a three phase system there are six voltage zeros per cycle, it is certain that there will be considerable asymmetry in the current flowing in at least one of the phases. If the fault occurs at any other point of the voltage wave, the resultant short-circuit is partially offset, that is to say, it contains a dc component of reduced magnitude.

The asymmetrical current consists of the symmetrical shortcircuit current superimposed on or offset by a dc component which decreases exponentially to practically zero within a few cycles. The asymmetrical short-circuit current peak determines the maximum mechanical stress to which the equipment may be subjected.

The maximum peak current is about 1.75 times the peak symmetrical current, or putting it another way $1.75 \times \sqrt{ }$, i.e. 2.5 times the rms value of the symmetrical short-circuit current.

Circuit breakers are selected so that the breaking capacity is always equal to or greater than the rms value calculated at the relevant point of installation. The making capacity is generally ignored, the assumption being that it will be in line with the level of peak current normally associated with the calculated rms current.

For example a circuit breaker with a breaking capacity of 15 kA rms will have a making capacity of $15 \times 2=30 \mathrm{kA}$ peak (see Table 32)

This assumes a short-circuit power factor of 0.3.

| Ratio $n$ between making and breaking capacity <br> Breaking <br> capacity $\mathrm{I}_{\mathrm{cn}}$ <br> (A) |  | Standard <br> power <br> factor |
| :--- | :--- | :--- | | Minimum making |
| :--- |
| capacity |
| $\left(\mathbf{n} \times \mathrm{I}_{\mathrm{cn}}\right)$ |

Table 32


Fig 17

## Calculation of Prospective Short Circuit Current

Several excellent proprietary computer programs are now available for calculating the prospective fault level at any point in the installation. They are also able to select the correct size and type of cable and match this with the correct circuit protective device.

## Estimation of Prospective Fault Current

Actually calculating prospective short-circuit current is not in itself difficult but it does require basic data which is not always available to the electrical installation designer.

It is therefore usual to use a simple chart as shown in Fig 18 to estimate the prospective short circuit current. This type of chart always gives a prospective fault level greater than that which would have been arrived at by calculation using accurate basic data. Therefore it is safe to use but sometimes may result in an over engineered system.

Conductor Cross Sectional Area (mm2) (Cu)


Fig 18


Fig 19

## Example

1 Project 40 m of cable length across on to the $240 \mathrm{~mm}^{2}$ cable curve. From this point project down onto the 28kA curve. From this point projecting across we note that the prospective fault level at the panelboard is 24 kA .

2 Project 60m of cable length across onto the $70 \mathrm{~mm}^{2}$ cable curve. From this point project down on to the 24 kA curve. From this point projecting across we see that the prospective fault level at the MCB distribution board is 10 kA .

Prospective Short Circuit Current in Domestic Installations


Fig 20
On single phase supplies up to 100A the electricity supply companies generally recommend that any installation is designed to cope with the maximum system fault level of the distributing main.

The declared fault level of the LV distributing main is $16 \mathrm{kA}(0.55 \mathrm{pf})$ Some supply companies do, however, accept that the impedance of the service cable may be taken into account as this is unlikely to change during the lifetime of the installation. The graph in Fig 20 shows for a standard service arrangement using a $25 \mathrm{~mm}^{2}$ service cable, the maximum prospective fault current at the consumer units incoming terminals, depending on the length of service cable from the point of connection to the LV distributing main.

The service cable length for domestic and similar installations may be taken as the distance from the service position in the consumer's premises to the boundary of the plot, assuming that the distributing mains cable is in the adjacent footpath.

Note: Hager consumer units with the following main incoming devices are tested to BS EN 60439-3 annex ZA 16kA conditional short circuit.

| Incoming device | Cat Ref |
| :--- | :--- |
| 63A 2P switch disconnector | SB263U |
| 100A 2P switch disconnector | SB299U |
| 63A 2P RCCB | CDC263U |
| $80+100$ 2 2P RCCB | CD, CN |
|  | $280 U+284 U$ |
| 40A 2P RCCB / Garage Boards | CDC240U |

Probable Short-Circuit Current


Fig 21

On page 3.43 the relationship between probable short-circuit current and service short-circuit breaking capacity is explained. The probable short circuit is the type of short circuit which is most likely to occur; this is nearly always at the extremity of the protected cable and more often than not a single phase or earth fault. Fig 21 shows a typical 3 phase 4 wire 400 V system fed by a 500 kVA transformer. The transformer is adjacent to the main switchboard so the prospective short-circuit current (PSCC) on the main switchboard busbars is estimated as 18 kA . The probable short-circuit current on the panelboard feeder circuit is estimated as 13 kA , if it were a 3 phase symmetrical fault, or 6.5 kA for a phase to neutral fault, which in fact would be the most likely type of fault. (Note: when estimating a phase to neutral prospective short-circuit current the length of conductor is doubled.)

Therefore for this application the main switchboard incoming circuit breaker
(A) Should have an $\mathrm{I}_{\mathrm{cs}} \geq 18 \mathrm{kA}$ and an $\mathrm{I}_{\mathrm{cu}} \geq 18 \mathrm{kA}$.

The panelboard feeder circuit breaker
(B) Should have an $\mathrm{I}_{\mathrm{cu}} \geq 18 \mathrm{kA}$ and an $\mathrm{I}_{\mathrm{cs}} \geq 13 \mathrm{kA}$.

Prospective Short Circuit Current (PSCC)

## Selectivity \& Discrimination

## Co-ordination between circuit protective devices

The proper co-ordination of two circuit protective devices is essential in all installations in order to fulfil the requirements of the Wiring Regulations which set out to ensure the safe continuity of supply of electrical current under all conditions of service. If a fault does occur, the circuit protective device nearest the fault should operate, allowing the device immediately upstream to continue to supply healthy circuits. This is called discrimination.

## Sometimes the upstream device is selected to protect the

 downstream device(s) against high prospective short circuit currents and will operate to provide this protection should the actual short circuit current rise to a level which cannot be handled by the device nearest the fault. This is called back-up protection and devices should be so chosen as to allow discrimination up to the point the back-up device takes over.
## Discrimination

Discrimination, which is sometimes called selectivity, is the co-ordination of two automatic circuit protective devices in such a way that a fault appearing at any given point in an installation is cleared by the protective device installed immediately upstream of the fault and by that device alone.


Fig 22
Example
A fault occurs downstream of final sub-circuit device "C". All other protective devices remain closed ensuring continuity of supply to the rest of the installation.

When this ideal situation is achieved under all conditions it is called "total discrimination".

Discrimination between two protective devices can be based on either the magnitude of the fault which is called "current discrimination" or the duration of the time the upstream device can withstand the fault current; this is called "time discrimination".

## Current discrimination

In order to achieve "current discrimination" in a distribution system it is necessary for the downstream device to have a lower continuous current rating and a lower instantaneous tripping value than the upstream device. Current discrimination increases as the difference between the continuous current ratings of the upstream and downstream devices increases.

A simple way of checking current discrimination at both overload and short-circuit conditions is to compare the time/current characteristic curves of both devices plotted to the same scale. Transparency overlays, if available, make this task much easier (see Fig 23). For this example the time/current characteristics of a 32A type 'B' circuit breaker complying with BS EN 60898, with a 100A category ' $A$ ' circuit breaker to BS EN 60947-2 are checked for current discrimination.

Because the thermal characteristic curve of the upstream circuit breaker clears the knee of the characteristic curve of the smaller downstream breaker, it can be said that overload discrimination is achieved under all conditions. However because the instantaneous characteristic curves cross at 0.01 sec , short-circuit discrimination is limited up to the point they cross, which in this case is approximately 2.7 kA . The point at which the two time/current characteristics cross is called the limit of discrimination or selectivity. In this example the level of discrimination $I_{s}$ is 2.7 kA , so we only have partial discrimination between these two devices.


Fig 23

## Time discrimination

Time discrimination is achieved by delaying the opening of the upstream circuit breaker until the downstream circuit breaker haopened and cleared the fault. The total clearing time of the
downstream circuit breaker must be less than the time setting of the upstream circuit breaker and the upstream circuit breaker must be able to withstand the fault current for the time setting period. Therefore the upstream circuit breaker must be a category ' $B$ ' breaker which has been designed and tested for this purpose.

To determine time discrimination it is only necessary to compare the time/current characteristic curves of the two devices to ensure that no overlap occurs.


Fig 24

## Short circuit discrimination

A more accurate way of checking the discrimination between two circuit protective devices at short circuit levels is to compare the energy let-through of the downstream device with the no-tripping or pre-arcing energy levels of the upstream device.

In order to check current discrimination at short circuit levels between:

Fuse upstream - fuse downstream
It is only necessary to compare the $I^{2} t$ values of each fuse. This information is usually available in very simple tabular form (see Table $33)$. If the total let-through energy $\left(1^{2} t\right)$ of the downstream fuse is less than the pre-arcing energy $\left(1^{2} \mathrm{t}\right)$ of the upstream fuse, then total discrimination is achieved at short-circuit levels.

Fuse $1^{2} t$ characteristics

| Fuse $\mathbf{l}^{2}$ t characteristics <br> Rated current <br> Amperes | Pre-arching $\mathbf{I}^{2} \mathbf{t}$ <br> $\mathbf{k A}^{2} \mathbf{s}$ | Total $\mathbf{I}^{2} \mathbf{t}$ <br> $\mathbf{k A}^{2} \mathbf{s}$ |
| :--- | :--- | :--- |
| 6 | 0.01 | 0.025 |
| 10 | 0.07 | 0.25 |
| 16 | 0.17 | 0.45 |
| 20 | 0.31 | 0.90 |
| 25 | 0.62 | 1.90 |
| 32 | 1.00 | 3.0 |
| 40 | 2.1 | 8.0 |
| 50 | 11 | 17 |
| 63 | 22 | 30 |
| 80 | 39 | 70 |
| 100 | 101 | 100 |
| 125 | 190 | 170 |
| 160 | 480 | 300 |
| 200 | 1100 | 500 |
| 315 | 1800 | 1100 |
| 400 |  | 2100 |
| 500 |  | 3100 |
| 630 |  | 5000 |
| 23 |  |  |

Table 33
MCB Total let-through energy

| MCB <br> In | Total let-through energy <br> kA2S at PSCC <br> 3kA | 6kA |  |
| :--- | :--- | :--- | :--- |
| 6 | 5.9 | 10.5 | 10 kA |
| 10 | 6.5 | 12.2 | 21.5 |
| 16 | 8.0 | 17.5 | 30 |
| 20 | 8.8 | 19.5 | 34 |
| 25 | 10 | 21 | 38 |
| 32 | 11 | 24 | 42 |
| 40 | 12.5 | 29 | 50 |
| 50 | 15 | 34 | 61 |
| 63 | 16 | 38 | 72 |
| Table 34 |  |  |  |

Fuse upstream - Circuit breaker downstream. The same procedure applies to fuse/circuit breaker as it does to fuse/fuse association to check current discrimination.

While for all practical purposes, a desk top study of time/current and let-through energy ( I 2 t ) characteristics are perfectly adequate, the British Standards for circuit breakers do recommend testing to confirm the results. With this in mind Hager have prepared a complete list of discrimination levels for all its circuit protective devices.


Fig 25 Back-up protection co-ordination


Fig 26

## Back-up protection

Sometimes known as cascading, when the energy limiting capacity of an upstream breaker is used to allow the use of a downstream circuit breaker having a short circuit breaking capacity $\left(I_{\mathrm{cu}}\right)$ lower than the prospective fault level at the point at which it is installed. Table 35 shows the prospective fault level achieved with cascading.

It should be noted that when two circuit protective devices are used in association to improve the short-circuit capacity of the downstream device, total selectivity can never be achieved up to the assigned breaking capacity of the association.

The upstream device must at some point operate to provide the necessary protection to the downstream circuit breaker. This point, which is known as the take-over current, must not be greater than the rated short-circuit capacity of the downstream circuit breaker alone. It therefore follows that the limit of selectivity $I_{s}$ will be less than the take-over current $\mathrm{I}_{\mathrm{B}}$. See Fig 25 .

Example
A panelboard is to be installed at a point where the prospective fault level is 25 kA . 250A incoming and 16A TP outgoing circuits. Select the lowest cost circuit breakers which may be used. See Fig 26.

Incoming - Hager H250 MCCB having an $\mathrm{I}_{\mathrm{cu}}$ of 40kA.
From Table 35 we see we can select a Hager H125 MCCB having an $\mathrm{I}_{\mathrm{cu}}$ of 16 kA to BS EN60947-2 but enhanced to 30kA with cascading.

## Co-ordination \& Selectivity



Fig 27

Circuit breaker to circuit breaker back-up protection

| Upstream device | 125A Frame <br> MCCB | 250A Frame <br> MCCB | 400A Frame <br> MCCB | 630A Frame <br> MCCB | 800A Frame <br> MCCB |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Downstream Device | 16 | 20 |  |  |  |
| 6kA MCBs MTN | 16 | 20 |  |  |  |
| 10kA MCBs NBN, NCN, NDN | 30 | 30 | 30 | 30 |  |
| 125A frame MCCB |  |  | 45 | 50 | 50 |
| 250A frame device |  |  | 50 | 50 |  |
| 400A frame device |  |  |  |  |  |
| 630A frame device |  |  |  |  |  |
| Please consult us |  |  |  |  |  |

Table 35

## Fuse to MCCB back-up protection

Upstream

| Downstream | Device <br> type | BS88 Gg <br> 250A | BS88 Gg <br> 315A | BS88 Gg <br> 400A | BS88 Gg <br> 630A | BS88 Gg <br> 800A | BS88 Gg <br> 1000A |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | 125A frame | 80 kA |  |  |  |  |  |
|  | 160A frame |  | 80 kA | 80kA |  |  |  |
|  | 250A frame |  |  | 80 kA | 80 kA |  |  |
|  | 400A frame |  |  |  | 80 kA | 80 kA |  |
|  | 630A frame |  |  |  |  |  |  |

Table 36

Prospective fault levels to which selectivity is achieved.

|  | NCN |  |  |  |  |  |  |  |  | NDN |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BS EN 947-2 | 10kA |  |  |  | 15kA |  |  |  |  | 10kA |  |  |  |  |  |  |  |  |
| Curve | C |  |  |  |  |  |  |  |  | D |  |  |  |  |  |  |  |  |
| In | 6A | 10A | 16A | 20A | 25A | 32A | 40A | 50A | 63A | 6A | 10A | 16A | 20A | 25A | 32A | 40A | 50A | 63A |
| MTN/NB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6A |  |  | 0.12 | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 |  | 0.15 | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 10A |  |  |  | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 |  |  | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 16A |  |  |  |  | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 |  |  |  |  | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 20A |  |  |  |  |  | 0.24 | 0.3 | 0.38 | 0.47 |  |  |  |  |  | 0.48 | 0.6 | 0.75 | 0.95 |
| 25A |  |  |  |  |  |  | 0.3 | 0.38 | 0.47 |  |  |  |  |  |  | 0.6 | 0.75 | 0.95 |
| 32A |  |  |  |  |  |  |  | 0.38 | 0.47 |  |  |  |  |  |  |  | 0.75 | 0.95 |
| 40A |  |  |  |  |  |  |  |  | 0.47 |  |  |  |  |  |  |  |  | 0.95 |
| NC/MLN |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0.5A | 0.05 | 0.08 | 0.12 | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 | 0.09 | 0.15 | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 1A | 0.05 | 0.08 | 0.12 | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 | 0.09 | 0.15 | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 2 A | 0.05 | 0.08 | 0.12 | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 | 0.09 | 0.15 | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 3 A | 0.05 | 0.08 | 0.12 | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 | 0.09 | 0.15 | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 4A |  | 0.08 | 0.12 | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 | 0.09 | 0.15 | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 6 A |  |  | 0.12 | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 |  | 0.15 | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 10A |  |  |  | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 |  |  | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 16A |  |  |  |  | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 |  |  |  |  | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 20A |  |  |  |  |  | 0.24 | 0.3 | 0.38 | 0.47 |  |  |  |  |  | 0.48 | 0.6 | 0.75 | 0.95 |
| 25A |  |  |  |  |  |  | 0.3 | 0.38 | 0.47 |  |  |  |  |  |  | 0.6 | 0.75 | 0.95 |
| 32 A |  |  |  |  |  |  |  | 0.38 | 0.47 |  |  |  |  |  |  |  | 0.75 | 0.95 |
| 40A |  |  |  |  |  |  |  |  | 0.47 |  |  |  |  |  |  |  |  | 0.95 |
| ND |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6A |  |  |  | 0.15 | 0.19 | 0.24 | 0.3 | 0.38 | 0.47 |  |  | 0.24 | 0.3 | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 10A |  |  |  |  |  | 0.24 | 0.3 | 0.38 | 0.47 |  |  |  |  | 0.38 | 0.48 | 0.6 | 0.75 | 0.95 |
| 16A |  |  |  |  |  |  |  | 0.38 | 0.47 |  |  |  |  |  | 0.48 | 0.6 | 0.75 | 0.95 |
| 20 A |  |  |  |  |  |  |  |  | 0.47 |  |  |  |  |  |  | 0.6 | 0.75 | 0.95 |
| 25A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.75 | 0.95 |
| 32A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 0.95 |

Table 37

## Circuit Breaker Discrimination Charts



| MCCB to MCCB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | H125 |  |  |  |  |  |  |  |  |  | H250 |  |  | H400 |  |  | H630 / H800 |  |  |  |
| In | A | 16 | 20 | 25 | 32 | 40 | 50 | 63 | 80 | 100 | 125 | 160 | 200 | 250 | 250 | 320 | 400 | 400 | 500 | 630 | 800 |
| H125 | 16 |  |  | 0.9 | 1 | 1 | 1 | 0.95 | 1 | 1.1 | 1.3 | 1.6 | 2 | 2.5 | 2.3 | 3 | 3.4 | 5.6 | 6.4 | 8.3 | 8.3 |
|  | 20 |  |  |  | 1 | 1 | 1 | 0.95 | 1 | 1.1 | 1.3 | 1.6 | 2 | 2.5 | 2.3 | 3 | 3.4 | 5.6 | 6.4 | 8.3 | 8.3 |
|  | 25 |  |  |  |  | 1 | 1 | 0.95 | 1 | 1.1 | 1.3 | 1.6 | 2 | 2.5 | 2.3 | 3 | 3.4 | 5.6 | 6.4 | 8.3 | 8.3 |
|  | 32 |  |  |  |  |  | 1 | 0.95 | 1 | 1.1 | 1.3 | 1.6 | 2 | 2.5 | 2.3 | 3 | 3.4 | 5.6 | 6.4 | 8.3 | 8.3 |
|  | 40 |  |  |  |  |  |  | 0.95 | 1 | 1.1 | 1.3 | 1.6 | 2 | 2.5 | 2.3 | 3 | 3.4 | 5.6 | 6.4 | 8.3 | 8.3 |
|  | 50 |  |  |  |  |  |  |  | 1 | 1.1 | 1.3 | 1.6 | 2 | 2.5 | 2.3 | 3 | 3.4 | 5.6 | 6.4 | 8.3 | 8.3 |
|  | 63 |  |  |  |  |  |  |  |  | 1.1 | 1.3 | 1.6 | 2 | 2.5 | 2.1 | 2.5 | 3.4 | 5.6 | 6.4 | 8 | 8 |
|  | 80 |  |  |  |  |  |  |  |  |  | 1.3 | 1.6 | 2 | 2.5 | 2 | 2.5 | 3.4 | 5.6 | 6.4 | 8 | 8 |
|  | 100 |  |  |  |  |  |  |  |  |  |  | 1.6 | 2 | 2.5 | 2 | 2.5 | 3.4 | 5.6 | 6 | 8 | 8 |
|  | 125 |  |  |  |  |  |  |  |  |  |  |  | 2 | 2.5 | 2 | 2.5 | 3.4 | 5.6 | 6 | 8 | 8 |
| H250 | 160 |  |  |  |  |  |  |  |  |  |  |  |  | 2.5 | 2 | 2.5 | 3.4 | 4 | 4 | 4.5 | 4.5 |
|  | 200 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.4 | 3.4 | 4 | 4 | 4.5 | 4.5 |
|  | 250 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.4 | 3.4 | 4 | 4 | 4.5 | 4.5 |
| H400 | 250 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.4 | 3.4 | 4 | 4 | 4 | 4 |
|  | 320 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3.4 | 4 | 4 | 4 | 4 |
|  | 400 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4 | 4 |
| H630 | 400 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 4.4 | 4.4 |
|  | 500 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 630 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 800 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Circuit Breaker $\mathrm{Z}_{\mathrm{s}}$ Values \&

Energy Let Through

| Earth loop impedance $\left(Z_{s}\right)$ values for MCBs \& MCCBs |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Below are the maximum permissible values of $Z_{s}$ to obtain disconnection in 0.4 \& 5 seconds |  |  |  |  |  |  |
| Type | Rated trip In | Max let-through energy (kA2s) at PSCC |  |  | Max Zs (ohms) |  |
|  |  |  |  |  | 0.4 | 5 |
|  |  | 3kA | 6kA | 10kA | Secs | Secs |
| MTN/ | 6 | 5.9 | 10.5 | 15 | 8 | 8.8 |
| NBN | 10 | 6.5 | 12.2 | 21.5 | 4.8 | 5.33 |
| B curve | 16 | 8.0 | 17.5 | 30 | 3 | 3.33 |
|  | 20 | 8.8 | 19.5 | 34 | 2.4 | 2.66 |
|  | 25 | 10 | 21 | 38 | 1.92 | 2.14 |
|  | 32 | 11 | 24 | 42 | 1.5 | 1.66 |
|  | 40 | 12.5 | 29 | 50 | 1.2 | 1.33 |
|  | 50 | 15 | 34 | 61 | 0.96 | 1.06 |
|  | 63 | 16 | 38 | 72 | 0.76 | 0.84 |
| NCN/HM | 0.5 | 0.01 | 0.01 | 0.01 | 48 | 120 |
| C curve | 1 | 4.0 | 7.0 | 10 | 24 | 53 |
|  | 2 | 4.0 | 7.0 | 10 | 12 | 26 |
|  | 3 | 5.0 | 10.0 | 15 | 8 | 18.78 |
|  | 4 | 5.9 | 10.5 | 15 | 6 | 13.56 |
|  | 6 | 5.9 | 10.5 | 15 | 4 | 8.8 |
|  | 10 | 6.5 | 12.2 | 21.5 | 2.4 | 5.33 |
|  | 16 | 8.0 | 17.5 | 30 | 1.5 | 3.33 |
|  | 20 | 8.8 | 19.5 | 34 | 1.2 | 2.66 |
|  | 25 | 10 | 21 | 38 | 0.96 | 2.14 |
|  | 32 | 11 | 24 | 42 | 0.75 | 1.66 |
|  | 40 | 12.5 | 29 | 50 | 0.6 | 1.33 |
|  | 50 | 15 | 34 | 61 | 0.48 | 1.06 |
|  | 63 | 16 | 38 | 72 | 0.38 | 0.84 |
|  | 80 |  |  |  | 0.30 | 0.66 |
|  | 100 |  |  |  | 0.24 | 0.53 |
| NDN | 6 | 5.9 | 10.5 | 15 | 2 | 8.8 |
| D curve | 10 | 6.5 | 12.2 | 21.5 | 1.2 | 5.33 |
|  | 16 | 8.0 | 17.5 | 30 | 0.75 | 3.33 |
|  | 20 | 8.8 | 19.5 | 34 | 0.6 | 2.66 |
|  | 25 | 10 | 21 | 38 | 0.48 | 2.14 |
|  | 32 | 11 | 24 | 42 | 0.37 | 1.66 |
|  | 40 | 12.5 | 29 | 50 | 0.3 | 1.33 |
|  | 50 | 15 | 34 | 61 | 0.24 | 1.06 |
|  | 63 | 16 | 38 | 72 | 0.19 | 0.84 |

## Table 40

| Type | Rated trip In | Max $Z$ 0.4 secs | $\begin{aligned} & 5 \\ & \text { secs } \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| H125 fixed mag. trip | 16 | 0.2 | 1.9 |
|  | 20 | 0.2 | 1.5 |
|  | 25 | 0.2 | 1.2 |
|  | 32 | 0.2 | 0.94 |
|  | 40 | 0.2 | 0.75 |
|  | 50 | 0.2 | 0.6 |
|  | 63 | 0.2 | 0.48 |
|  | 80 | 0.2 | 0.38 |
|  | 100 | 0.2 | 0.3 |
|  | 125 | 0.2 | 0.24 |
| H 250 mag. trip set to max | 160 | 0.125 | 0.125 |
|  | 200 | 0.10 | 0.10 |
|  | 250 | 0.08 | 0.08 |
| H 250 mag. trip set to min | 160 | 0.25 | 0.25 |
|  | 200 | 0.20 | 0.20 |
|  | 250 | 0.16 | 0.16 |
| H 400 mag. trip set to max | 320 | 0.06 | 0.06 |
|  | 400 | 0.05 | 0.05 |
| H 400 mag. trip set to min | 320 | 0.13 | 0.13 |
|  | 400 | 0.10 | 0.10 |
| H 800 mag. set to max | 500 | 0.05 | 0.05 |
|  | 630 | 0.03 | 0.03 |
|  | 800 | 0.03 | 0.03 |
| H 800 mag. trip set to min | 500 | 0.10 | 0.10 |
|  | 630 | 0.06 | 0.06 |
|  | 800 | 0.05 | 0.05 |

Table 41

These values have been calculated using the formula
$Z_{s}=$ Uoc/la taken from appendix 3 of BS EN7671: 1992, taking into account the $20 \%$ tolerance stated in section 8.3.3.1.2 of BS EN 60947-2. Uoc is the open circuit voltage of the REC transformer taken at 240 V . la is the current causing operation of the protective device within the specified time. Calculate from $\operatorname{Im} \times 1.2$.

Full table as Apps guide (Table 27)

Single module RCBO characteristics

- Single pole overcurrent protection
- Single pole switching (solid neutral)
- Positive contact indication
- Neutral lead - 700 mm long

| Current rating | Ambient temperature ( ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $30^{\circ} \mathrm{C}$ | $35^{\circ} \mathrm{C}$ | $40^{\circ} \mathrm{C}$ | $45^{\circ} \mathrm{C}$ | $50^{\circ} \mathrm{C}$ | $55^{\circ} \mathrm{C}$ | $60^{\circ} \mathrm{C}$ |
| 6A | 6 | 5.9 | 5.8 | 5.7 | 5.6 | 5.5 | 5.4 |
| 10A | 10 | 9.8 | 9.7 | 9.5 | 9.3 | 9.2 | 9.0 |
| 16A | 16 | 15.7 | 15.5 | 15.2 | 14.9 | 14.7 | 14.4 |
| 20A | 20 | 19.7 | 19.3 | 19.0 | 18.7 | 18.3 | 18.0 |
| 25A | 25 | 24.6 | 24.2 | 23.8 | 23.3 | 22.9 | 22.5 |
| 32A | 32 | 31.5 | 30.9 | 30.4 | 29.9 | 29.3 | 28.8 |
| 40A | 40 | 39.3 | 38.6 | 38.0 | 37.3 | 36.6 | 36.0 |
| 45A | 45 | 44.2 | 43.5 | 42.8 | 42.0 | 41.2 | 40.5 |
| 50A | 50 | 49.2 | 48.3 | 47.5 | 46.7 | 45.8 | 45.0 |

## Technical specification

Standard / approvals: BS EN61009
Type tested KEMA up to 50A
ASTA up to 40A
Nominal voltage:
127/230VAC (-6\% +10\%)
$50 / 60 \mathrm{~Hz}$
$10 \mathrm{~mA} / 30 \mathrm{~mA}$ - AC
6 kA or 10 kA (on request)
Working -5OC to +400 C
Storage -50OC to $+800 C$
Trip free
Electrical - 4000
Mechanical - 20000

Fuse carriers - characteristics


## Connection capacity:

- Top: $16 \square$ Rigid conductor
- Bottom: 10 Flexible conductor
or busbar
Table 42


## RCCBs

## Residual current devices

A residual current device (RCCB) is the generic term for a device which simultaneously performs the functions of detection of the residual current, comparison of this value with the rated residua operating value and opening the protected circuit when the residua current exceeds this value.

For fixed domestic installations and similar applications we have two types:

- Residual current operated circuit-breaker without integral over-current protection (RCCB's) which should comply with the requirements of BS EN 61008
- Residual current operated circuit-breaker with integral over-current protection (RCBO's) which should comply with the requirements of BS EN 61009

Both RCCB's and RCBO's are further divided into types depending on their operating function :-

Type AC For which tripping is ensured for residual sinusoidal alternating currents, whether suddenly applied or slowly rising. Marked with the symbol.


Type A For which tripping is ensured for residual sinusoidal alternating currents and residual pulsating direct currents, whether suddenly applied or slowly rising. Marked with the symbol.


Type S For selectivity, with time-delay. Marked with the symbol.

## S

RCCB's must be protected against short-circuits by means of circuit-breakers or fuses. RCBO's have their own in built short-circuit protection, up to it's rated value.

The drawing opposite shows how a torroid is located around the line and neutral conductors to measure the magnetic fields created by the current flowing in these conductors. The sum of the magnetic fields set up by these currents (which takes into consideration both the magnitude and phase relationship of the currents) is detected by the torroid.

In a normal healthy circuit the vector sum of the current values added together will be zero. Current flowing to earth, due to a line earth fault, will return via the earth conductor, and regardless of load conditions will register as a fault. This current flow will give rise to a residual current (Ires) which will be detected by the device.

It is most important that the line and neutral conductors are passed through the torroid. A common cause of nuisance operation is the failure to connect the neutral through the device.

RCCBs work just as well on three phase or three phase and neutral circuits, but when the neutral is distributed it must pass through the torroid.

RCCBs are not suitable for use on dc systems and unearthed networks.

## RCCBs - domestic installation

RCCBs can be installed in two ways:

1. Whole house protection.
2. Selective protection.

Whole house protection is provided typically by a consumer unit where the RCCB device serves as the main switch. Although very popular this suffers from a disadvantage: all circuits are disconnected in the event of fault. Selective protection can be provided by associating the RCCB with identified high risk circuits by adopting one or more of the following:

## Principle



Fig 28
Current flowing through torroid in healthy circuit

$$
I_{\text {res }}=I_{1}-I_{2}=0
$$

Current flowing through torroid in circuit with earth fault $\mathrm{I}_{3}$

$$
I_{\text {res }}=I_{1}-I_{2}+I_{3}=I_{3}
$$

- Split busbar consumer unit:

All circuits are fed via an overall isolator and selected circuits fed additionally via the RCCB. Typical circuits fed direct are lighting, freezer, storage heating: and circuits fed via the RCCB are socket outlets, garage circuits. This concept minimises inconvenience in the event of fault.

## Individual RCBO

each separate final circuit requiring protection by a RCD can be supplied through an RCBO. This method provides the best solution for minimising inconvenience

## Nuisance Tripping

All Hager RCCBs incorporate a filtering device preventing the risk of nuisance tripping due to transient voltages (lightning, line disturbances on other equipment...) and transient currents (from high capacitive circuit).

## Pulsating DC Fault Current Sensitive

Increasingly, semi-conductors are also extensively used in computers, VDUs, printers, plotters... all of which may be fed from the mains electrical supply. The presence of semi-conductors may result in the normal sinusoidal ac waveform being modified. For example, the waveform may be rectified or, as in asymmetric phase control devices, the waveform may be chopped. The resulting waveforms are said to have a pulsating dc component.

In the event of an earth fault occurring in equipment containing semi-conductor devices, there is a probability that the earth fault current will contain a pulsating dc component.

Standard type AC may not respond to this type of earth fault current and the intended degree of protection will not be provided.

## Use of RCCBs

RCCBs offer excellent protection against earth fault currents; the main areas of application being as follows:

- $Z_{s}$ value too high to allow disconnection in the required time Where the overcurrent protection or a circuit breaker cannot provide disconnection within the specified time because the earth fault loop impedance is too high the addition of RCCB protection may well solve the problem without any other change in the system. Because of its high sensitivity to earth fault current and its rapid operating time, in most cases the RCCB will ensure disconnection within the specified time. This is achieved without any detriment to overcurrent discrimination because, unlike the situation in a fuse based system, the increased sensitivity is obtained without increasing sensitivity to overcurrent faults. Use of RCCBs in this way can be particularly useful for construction sites and bathrooms where disconnection times are more stringent than for standard installations. (Construction sites - 0.2s at $220-277 \mathrm{~V}$, bathrooms -0.4 s ).

The limitation to this technique is the requirement that the rated residual operating current multiplied by Zs should not exceed 50V. This is to avoid the danger of exposed conductive parts reaching an unacceptably high voltage level.

Residual current protection can even be added to a completed distribution system where the value of Zs is excessive, either because of a design oversight or subsequent wiring modification.

- Protection against shock by direct contact

So far we have considered shock by indirect contact only. Direct contact is defined thus:

Direct contact - contact of persons or livestock with live parts which may result in electric shock. The consideration here is not the hazard of parts becoming live as a result of a fault but the possibility of touching circuit conductors which are intentionally live.

RCCBs, although affording good protection against the potentially lethal effects of electric shock, must not be used as a the sole means of protection against shock by direct contact. The Electricity at Work Act recommends the use of RCCBs, "....danger may be reduced by the use of a residual current device but states that this should be ".... considered as a second line of defence". The Wiring Regulations defines the other measures that should be taken i.e.

- Insulation of live parts.
- Barriers or enclosures.
- Obstacles.
- Placing live parts out of reach.

Additionally an RCCB used for this purpose should have:

- A sensitivity of 30 mA
- An operating time not exceeding 40 mS at a residual current of 150 mA .

The specified sensitivity is based on research that has been carried out to estimate the effect various levels and duration of current can have on the human body. This experience is summarised in a graph shown in 'IEC 479-1: Effects of current passing through the human body'. A simplified version of this graph is shown opposite. It shows that very small currents can be tolerated for reasonably long periods and moderate currents for very short periods. It can be seen, for instance, that 100 mA for 100 mS or 20 mA for 500 mS will not normally cause any harmful effect. 200 mA for 200 mS or 50 mA for 500 mS which are in Zone 3, would be more dangerous; and shock levels in Zone 4 carry a risk of lethal consequences.

The tripping characteristic for a 30 mA RCCB is also shown in the graph. It shows the level of current required to cause the RCCB to trip, for example; 50 mA will cause a trip but not 10 mA . Comparing its characteristic with the various zones on the graph it can be seen that the 30 mA RCCB gives a very good measure of protection against the hazards associated with electric shock. Where a higher level of protection is required, for example in laboratories, 10 mA devices are available.


Fig 29

## Note:

Although RCCBs are extremely effective devices they must never be used as the only method of protection against electric shock. With or without RCCB protection all electrical equipment should be kept in good condition and should never be worked on live.

## - Protection against shock outside the equipotential bonding

 zoneBonding conductors are used in an installation to maintain metallic parts, as near as possible, to the same potential as earth. Working with portable equipment outside this equipotential bonding zone, e.g. in the car park of a factory, introduces additional shock hazards. Socket outlets rated 32A or less 'which may be reasonably expected to supply portable equipment for use outdoors' be equipped with 30 mA RCCB protection unless fed from an isolating transformer or similar device, or fed from a reduced voltage.

## - Protection in special locations

The use of RCCBs is obligatory or recommended in the following situations:

- Caravans: 30 mA RCCBs should be used.
- TT systems.
- Swimming pools: 30mA RCCB for socket outlets in Zone B obligatory; recommended in Zone C.
- Agricultural and horticultural: 30mA RCCB for socket outlets and for the purpose of protection against fire, RCCB $\leq 0.5 A$ sensitivity.
- Construction sites: 30mA RCCB recommended.


## - Portable equipment

With the exception mentioned above, where a socket is specifically designated for work outside the equipotential bonding zone, the Wiring Regulations demand the use of RCCBs to protect the users of portable equipment. It is widely recognised that their use has made a significant contribution to safety in the workplace and the home.

- Protection against fire hazards

The provisions in the Wiring Regulations for protection against shock by indirect contact ensure rapid disconnection under earth fault assuming the fault has negligible impedance. Under such conditions the fault current, as we have seen, is sufficiently great to cause the overcurrent protection device to quickly disconnect the fault. However high impedance faults can arise where the fault current is sufficient to cause considerable local heat without being high enough to cause tripping of the overcurrent protective device. The heat generated at the point of the fault may initiate a fire long before the fault has deteriorated into a low impedance connection to earth.

The provision of residual current protection throughout a system or in vulnerable parts of a system will greatly reduce the hazard of fire caused by such faults.

## - PEN conductors

The use of RCCBs with PEN conductors is prohibited. A PEN conductor is a single conductor combining the functions of neutral conductor and protective conductor. This being so, when the PEN conductor is taken through the torroid of an RCCB, earth faults will go undetected because the return path for the earth fault current is included in the residual sum.

## - Auxiliary contacts

A range of auxiliaries, alarm and shunt contacts are available for Hager RCCBs.

## - Supply entry

Top or bottom feed.

## CB/RCCB co-ordination

|  |  |  | With M | 's |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Short circuit |  | NBN | NCN | NDN |
| RCCB | current capacity of the RCCB only | $\begin{aligned} & 6-63 A \\ & \text { B } \end{aligned}$ | $\begin{aligned} & 6-63 A \\ & \text { B } \end{aligned}$ | $\begin{aligned} & \text { 6-63A } \\ & C \end{aligned}$ | $\begin{aligned} & 6-63 A \\ & \text { D } \end{aligned}$ |
| 2 poles |  |  |  |  |  |
| 16A | 1500A | 6kA | 10kA | 10kA | 6kA |
| 25A | 1500A | 6kA | 10kA | 10kA | 6kA |
| 40A | 1500A | 6kA | 10kA | 10kA | 6kA |
| 63A | 1500A | 6kA | 10kA | 10kA | 6kA |
| 80A | 1500A | 6kA | 10kA | 10kA | 6kA |
| 100A | 1500A | 6kA | 10kA | 10kA | 6kA |
| 4 poles |  |  |  |  |  |
| 16A | 1500A | 6kA | 6kA | 6kA | 4.5kA |
| 25A | 1500A | 6kA | 6kA | 6kA | 4.5 kA |
| 40A | 1500A | 6kA | 6kA | 6kA | 4.5 kA |
| 63A | 1500A | 6kA | 6kA | 6kA | 4.5 kA |
| 80A | 1500A | 6kA | 6kA | 6kA | 4.5 kA |
| 100A | 1500A | 6kA | 6kA | 6kA | 4.5kA |

Table 43

| RCCB | Short circuit current capacity of the RCCB only | With BS 1361 fuses |  |  | With BS 88 fuse |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 60A | 80A | 100A | 60A | 80A | 100A |
| 2P |  |  |  |  |  |  |  |
| 16A | 1500A | 13kA | 6kA | 3.5 kA | 11kA | 5kA | 3kA |
| 25A | 1500A | 13kA | 6kA | 3.5 kA | 11kA | 5kA | 3kA |
| 40A | 1500A | 13kA | 6kA | 3.5 kA | 11kA | 5kA | 3 kA |
| 63A | 1500A | 13 kA | 6kA | 3.5 kA | 11kA | 5 kA | 3kA |
| 80A | 1500A | 13kA | 6kA | 3.5 kA | 11kA | 5 kA | 3 kA |
| 100A | 1500kA | 13 kA | 6kA | 3.5 kA | 11kA | 5kA | 5 kA |
| 4 P |  |  |  |  |  |  |  |
| 16A | 1500A | 13kA | 6kA | 3.5 kA | 11kA | 5 kA | 3kA |
| 25A | 1500A | 13kA | 6kA | 3.5 kA | 11kA | 5kA | 3kA |
| 40A | 1500A | 13kA | 6kA | 3.5 kA | 11kA | 5kA | 3 kA |
| 63A | 1500A | 13 kA | 6kA | 3.5 kA | 11kA | 5kA | 3kA |
| 80A | 1500A | 13kA | 6kA | 3.5 kA | 11kA | 5kA | 3 kA |
| 100A | 1500A | 13kA | 6kA | 3.5 kA | 11kA | 5kA | 3kA |

Table 44

## Add-On Block

## RCCB Add-Ons

3 sensitivities $30 \mathrm{~mA}, 100 \mathrm{~mA} \& 300 \mathrm{~mA}$ instantaneous. 2 sensitivities $100 \mathrm{~mA} \& 300 \mathrm{~mA}$ time delayed.
RCCB add-ons can be associated with devices rated from 0.5 to 63A in 2 and 4 poles.

## Wiring Diagram



## Connection capacity


$33 A=25 \mathrm{~mm}^{2}$

## Characteristics

Easy coupling (drawer system)
Easy disassembly (without damage)
Conforms to EN61009 Appendix G

MCB \& RCCB add-on association chart

|  | 2 Pole |  |  | 4 Pole |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In | $\leq 63 \mathrm{~A}$ |  |  | $\leq 63 \mathrm{~A}$ |  |  |
| Sensitivity | 30mA | 100mA | 300mA | 30 mA | 100mA | 300mA |
| Cat Ref. (standard) | BD264 | BE264 | BF264 | BD464 | BE464 | BF464 |
| Cat Ref. (time delayed) |  | BN264 | BP264 |  | BN464 | BP464 |
| MCB suitability NBN | 6-63A | 6-63A | 6-63A | 6-63A | 6-63A | 6-63A |
| NCN | 0.5-63A | 0.5-63A | 0.5-63A | 0.5-63A | 0.5-63A | 0.5-63A |
| NDN | 0.5-63A | 0.5-63A | 0.5-63A | 0.5-63A | 0.5-63A | 0.5-63A |
| Width when combined with MCB |  | 4 module 70 mm |  |  |  | 7 module 122.5 mm |

Table 45

## Mounting



Fig 31

## Technical specifications

|  | Non-Adjustable |  | Adjustable |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | HR400 | HR402 | HR403 | HR410 | HR411 | HR420 | HR425 | HR440 | HR441 |
| Supply voltage $\sim 50 / 60 \mathrm{HZ}$ | 220-240V |  |  |  |  |  |  |  |  |
| Residual voltage $\sim 50 / 60 \mathrm{~Hz}$ | 500V Maximum |  |  |  |  |  |  |  |  |
| Power Absorbed | 3VA |  | 5VA |  |  |  |  |  |  |
| Output | Volt free contacts |  |  |  |  |  |  |  |  |
| Contact Rating | 6A / 250V AC-1 |  |  |  |  |  |  |  |  |
| Sensitivity I $\triangle$ n | 0.03A / 0.1A / 0.3A / 1A / 3A / 10A |  |  |  |  |  |  |  | $\begin{aligned} & 0.03 \mathrm{~A} / 0.1 \mathrm{~A} / 0.3 \mathrm{~A} \\ & 0.5 \mathrm{~A} / 1 \mathrm{~A} / 3 \mathrm{~A} / 10 \mathrm{~A} \end{aligned}$ |
| Instantaneous / Time Delay | Instantaneous |  |  | Instantaneous or time delay $0.13 \mathrm{~s} /$ $0.3 \mathrm{~s} / 1 \mathrm{~s} / 3 \mathrm{~s}$ |  |  | Instantan <br> time del $0.1 \mathrm{~s} / 0 .$ / 0.5s | $\begin{aligned} & \text { eoous or } \\ & \text { ay } \mathrm{s} / \\ & 3 \mathrm{~s} / 0.45 \mathrm{~s} \end{aligned}$ | Instantaneous or time dealy $0 \mathrm{~s} / 0.1 \mathrm{~s}$ / 0.3s / 0.5s / 0.75s /1s |
| Torroid Withstand Capacity | 50kA / 0.2s |  |  |  |  |  |  |  |  |
| Distance between torroid and relay | 50 Meter Maximum |  |  |  |  |  |  |  |  |
| Relay cable connection <br> - Rigid <br> - Flexible | $\begin{aligned} & 1.5 \square \text { to } 10 \square \\ & 1 \square \text { to } 6 \square \end{aligned}$ |  |  |  |  |  |  |  |  |
| Torroid cable connection <br> - Rigid <br> - Flexible | $\begin{aligned} & 1.5 \square \text { to } 4 \square \\ & 1 \square \text { to } 2.5 \square \end{aligned}$ |  |  |  |  |  |  |  |  |
| Relay Working temperature | $-10^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$ |  | $-5^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
| Storage temperature | $-25^{\circ} \mathrm{C}$ to $+40^{\circ} \mathrm{C}$ |  | $-25^{\circ} \mathrm{C}$ to $+40^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
| Torroid Working temperature | $-10^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |  | $-10^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |  |  |  |  |  |  |
| Storage temperature | $-40^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |  | $-40^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$ |  |  |  |  |  |  |

Table 46

## Main Characteristics

## "Reset" Button

When pressed, the output remains switched and return to normal is obtained by either: by pressing the "reset" clear pushbutton or cutting off the power supply. If the "reset" button is not pressed the device remains in the fault position.

## Test Button

Pressing the test button allows a fault simulation which operates the relay and the output contacts. The fault level display is shown by an LED on the front of the product.

## I $\Delta \mathrm{n}$ selector

Sensitivity setting: 0.03A instantaneous
$0.1 \mathrm{~A} / 0.3 \mathrm{~A} / 1 \mathrm{~A}$ and 3A time delay

## Time delay selector

Adjustable time setting - instantaneous $/ 0.13 \mathrm{~s} / 0.3 \mathrm{~s} / 1 \mathrm{~s}$ and 3 s


## Sealable settings

A sealable cover prevents interference once the settings have been made.

## Standard output (1 C/O contact)

Switching to state 1 on:

- Failure of the core/relay connection
- Fault current in the monitored installation


## Positive safety outlet (1 C/O contact)

Switching to state 1: Switching on the power
Switching to state 0: Failure of the core/relay connection fault current in the monitored installation failure of relay supply internal failure of relay

Optical scale display by 5 LEDs of the fault in \% of I $\Delta n$ Optical scale display by (5 LEDs) of the fault in \% of $I \Delta n$ Common pin 6:
State 1 : output terminal 8
State 0 : output terminal 4

1. Reset push button
2. Test push button
3. Fault signal LED
4. Device on indicator
5. Sensitivity setting
6. Time delay setting
7. Standard output
8. Safety output
9. Prealarm output
10. Remore reset
11. Optical scale

Circular Torroids HR800


## Circular Torroids



Fig 33

| Reference | Type | Dimensions (mm) |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | A | B | C | D | E |
| HR801 | $\varnothing 35$ | 35 | 92 | 86 | 43.5 | 74 |
| HR802 | $\varnothing 70$ | 70 | 115 | 118 | 60.5 | 97 |
| HR803 | $\varnothing 105$ | 105 | 158 | 162.5 | 84.5 | 140 |
| HR804 | $\varnothing 140$ | 140 | 218 | 200 | 103.5 | 183 |
| HR805 | $\varnothing 210$ | 210 | 290 | 295 | 150 | 265 |

Table 47

Rectangular Torroids

| Reference | Type | Dimensions (mm) |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  | A1 | A2 | B | C | D | E | F | G | H |
| HR830 | $70 \times 175$ | 70 | 175 | 176 | 260 | 85 | 225 | 22 | 40 | 7.5 |
| HR831 | $115 \times 305$ | 115 | 305 | 239 | 400 | 116 | 360 | 25 | 50 | 8.5 |
| HR832 | $150 \times 350$ | 150 | 350 | 284 | 460 | 140 | 415 | 28 | 50 | 8.5 |

Table 48


Fig 34

Rectangular Torroids

| Reference | A1 | A2 | B | C | D | E |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| FR820 | 20 | 30 | 89 | 110 | 41 | 32 |
| HR821 | 50 | 80 | 114 | 145 | 50 | 32 |
| HR822 | 80 | 80 | 145 | 145 | 50 | 32 |
| HR823 | 80 | 121 | 145 | 185 | 50 | 32 |
| HR824 | 80 | 161 | 184 | 244 | 70 | 46 |



## Mounting of Circular Torroids

| With Cables <br> Type of Torroid <br> $\varnothing$ |  | U 1000 R2V Single pole | U 1000 R2V Single pole | U 1000 R2V Multi pole | U 1000 R2V multi pole | U 1000 R2V multi pole | H07 V－U single pole | H07 V－U single pole |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | HR800 | $4 \times 16 \square$ | $2 \times 50 \square$ | 35ロ | 35ロ | 50ロ | $4 \times 35 \square$ | $2 \times 70 \square$ |
| 35 | HR801 | $4 \times 25 \square$ | $2 \times 70 \square$ | 50ロ | 35■ | $70 \square$ | $4 \times 50 \square$ | $2 \times 95 \square$ |
| 70 | HR802 | $4 \times 185 \square$ | $2 \times 400 \square$ or $4 \times 150 \square$ | 240ロ | 35■ | 300ロ | $4 \times 240 \square$ | $2 \times 400 \square$ or $4 \times 185 \square$ |
| 105 | HR803 | $4 \times 500 \square$ | $2 \times 630 \square$ or $4 \times 185 \square$ | 300■ | 35■ | 300ロ | $4 \times 400 \square$ | $2 \times 400 \square$ or $4 \times 240 \square$ |
| 140 | HR804 | $4 \times 630 \square$ | $2 \times 630 \square$ or $4 \times 240 \square$ | 300ロ | 35 $\square$ | 300ロ | $4 \times 400 \square$ | $2 \times 400 \square$ or $4 \times 240 \square$ |
| 210 | HR805 | $4 \times 630 \square$ | $2 \times 630 \square$ or $4 \times 240 \square$ | 300ロ | 35■ | 300ロ | $4 \times 400 \square$ | $2 \times 400 \square$ or $4 \times 240 \square$ |
| $70 \times 175$ | HR830 | $4 \times 630 \square$ | $2 \times 630 \square$ or $4 \times 240 \square$ | 300ロ | 35 | 300ロ | $4 \times 400 \square$ | $2 \times 400 \square$ or $4 \times 240 \square$ |
| $115 \times 305$ | HR831 | $4 \times 630 \square$ | $2 \times 630 \square$ or $4 \times 240 \square$ | $300 \square$ | 35■ | $300 \square$ | $4 \times 400 \square$ | $2 \times 400 \square$ or $4 \times 240 \square$ |
| $150 \times 350$ | HR832 | $4 \times 630 \square$ | $2 \times 630 \square$ or $4 \times 240 \square$ | 300■ | 35■ | 300ロ | $4 \times 400 \square$ | $2 \times 400 \square$ or $4 \times 240 \square$ |
| $20 \times 30$ | HR820 | $4 \times 16 \square$ | $2 \times 70 \square$ | $10 \square$ | 35 | 16ロ | $4 \times 10 \square$ | $2 \times 35 \square$ |
| $50 \times 80$ | HR821 | $4 \times 240 \square$ | $2 \times 630$ or $4 \times 185 \square$ | 120■ | 35■ | 150■ | $4 \times 185 \square$ | $2 \times 240 \square$ |
| $80 \times 80$ | HR822 | $4 \times 500 \square$ | $2 \times 630$ or $4 \times 185 \square$ | $300 \square$ | 35■ | $300 \square$ | $4 \times 400 \square$ | $2 \times 400$ or $4 \times 240 \square$ |
| $80 \times 120$ | HR823 | $4 \times 630 \square$ | $2 \times 630$ or $4 \times 240 \square$ | 300ロ | 35■ | 300ロ | $4 \times 400 \square$ | $2 \times 400$ or $4 \times 240 \square$ |
| $80 \times 160$ | HR824 | $4 \times 630 \square$ | $2 \times 630$ or $4 \times 240 \square$ | 300ロ | 35 $\square$ | 300ロ | $4 \times 400 \square$ | $2 \times 400$ or $4 \times 240 \square$ |

## Selectivity / Discrimination

Typical RCCB Time/Current Characteristics


Discrimination between Circuit Breakers with add on RCCBs
Having decided on the type and the limit of discrimination of the circuit breakers in the system, it is very important to consider the discrimination between any add on RCCBs. In theory it is possible to achieve current discrimination between RCCBs but the limit of discrimination is too low for practical purposes. Time discrimination is by far the best method and is achieved by delaying the tripping of the upstream RCCB, See Fig 36, which shows the RCCB characteristics for both instantaneous and time delayed.

Note that the limit of discrimination is the instantaneous setting of the associated circuit breaker. In other words if the earth fault current is greater than the instantaneous trip setting of the associated circuit breaker, the circuit breaker will trip regardless of the time delay on the RCCB. Table 49 indicates how time discrimination may be achieved between RCCBs.

Fig 36

Discrimination between Residual Current Devices


## Surge Protection Devices

|  | Class II - overvoltage protection |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | High | Medium |  |  |  | Fine |
| Reference | SPN140D | SPN215D | SPN215R | SPN415D | SPN415R | SPN208S |
| Installation exposure level (risk) | High | Medium | Medium | Medium | Medium | Low |
| Installation of SPD <br> Number of poles <br> Number of Modules <br> Nominal current | Parallel 1P 1 | $\begin{aligned} & \text { Parallel } \\ & 1 P+N \\ & 2 \\ & - \end{aligned}$ | $\begin{aligned} & \text { Parallel } \\ & 1 P+N \\ & 2 \\ & - \end{aligned}$ | Parallel 3P\&N <br> 4 <br> - | Parallel 3P\&N <br> 4 | $\begin{aligned} & \text { Series } \\ & 1 P+N \\ & 2 \end{aligned}$ |
| Nominal Voltage Un (V) Frequency (Hz) | $\begin{aligned} & \hline 230 \\ & 50 / 60 \end{aligned}$ | $\begin{aligned} & 230 \\ & 50 / 60 \end{aligned}$ | $\begin{aligned} & \hline 230 \\ & 50 / 60 \end{aligned}$ | $\begin{aligned} & 400 \\ & 50 / 60 \end{aligned}$ | $\begin{aligned} & 400 \\ & 50 / 60 \end{aligned}$ | $\begin{aligned} & 230 / 400 \\ & 50 / 60 \end{aligned}$ |
| Max. continuous operating Voltage Uc (V) common mode differential mode - | 275 | 275 | 275 | 275 | 275 | $\begin{aligned} & 440 \\ & 255 \end{aligned}$ |
| Voltage protection level Up (kV) common mode differential mode - | 1.2 | 1.0 | 1.0 | 1.0 | 1.0 | $\begin{aligned} & 1.2 \\ & 1.0 \end{aligned}$ |
| Discharge current wave 8/20us (kA) Nominal current In Maximum current Imax | $\begin{aligned} & 15 \\ & 40 \end{aligned}$ | $\begin{aligned} & 5 \\ & 15 \end{aligned}$ | $\begin{aligned} & 5 \\ & 15 \end{aligned}$ | $\begin{aligned} & 5 \\ & 15 \end{aligned}$ | $\begin{aligned} & 5 \\ & 15 \end{aligned}$ | $\begin{aligned} & 2 \\ & 8 \end{aligned}$ |
| Operating temperature range Storage temperature range | $\begin{aligned} & -40 /+60 \\ & -40 /+70 \end{aligned}$ | $\begin{aligned} & -40 /+60 \\ & -40 /+70 \end{aligned}$ | $\begin{aligned} & -40 /+60 \\ & -40 /+70 \end{aligned}$ | $\begin{aligned} & -40 /+60 \\ & -40 /+70 \end{aligned}$ | $\begin{aligned} & -40 /+60 \\ & -40 /+70 \end{aligned}$ | $\begin{aligned} & -40 /+60 \\ & -40 /+70 \end{aligned}$ |
| Short circuit withstand with max. backup fuse or MCB <br> Max. backup fuse Backup MCB (C curve) | $\begin{aligned} & 20 \mathrm{kA} \\ & 25 \mathrm{~A} \\ & 25 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 10 \mathrm{kA} \\ & 10 \mathrm{~A} \\ & 25 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 10 \mathrm{kA} \\ & 10 \mathrm{~A} \\ & 25 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 10 \mathrm{kA} \\ & 10 \mathrm{~A} \\ & 25 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 10 k A \\ & 10 \mathrm{~A} \\ & 25 \mathrm{~A} \end{aligned}$ | 6kA <br> 25A <br> 25A |
| End of life indication (fault indication) <br> 1. three stage indication-green, green/red, red (R versions) <br> 2. Basic indication - green/red (D versions) <br> 3. Green LED is on when SPD is working | Yes <br> N/A <br> N/A | N/A <br> Yes <br> N/A | Yes <br> N/A <br> N/A | N/A <br> Yes <br> N/A | Yes <br> N/A <br> N/A | N/A <br> N/A <br> Yes |
| Applications industrial \& commercial buildings domestic buildings | Yes <br> Yes | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | $\begin{aligned} & \text { Yes } \\ & \text { Yes } \end{aligned}$ | Yes <br> Yes | Yes Yes | Yes <br> Yes |
| Connection capacity | $2.5 / 35$ $\mathrm{mm}^{2}$ | $\begin{aligned} & 2.5 / 25 \\ & \mathrm{~mm}^{2} \end{aligned}$ | $\begin{aligned} & 2.5 / 25 \\ & \mathrm{~mm}^{2} \end{aligned}$ | $\begin{aligned} & 2.5 / 25 \\ & \mathrm{~mm}^{2} \end{aligned}$ | $\begin{aligned} & 2.5 / 25 \\ & \mathrm{~mm}^{2} \end{aligned}$ | $\begin{aligned} & \hline 2.5 / 10 \\ & \mathrm{~mm}^{2} \end{aligned}$ |
| Connection capacity for the auxiliary contact | N/A | N/A | $\begin{aligned} & 0.5 / 1.5 \\ & \mathrm{~mm}^{2} \end{aligned}$ | N/A | $0.5 / 1.5$ <br> $\mathrm{mm}^{2}$ | N/A |
| Auxiliary contact <br> Voltage/nominal current | N/A | N/A | $\begin{aligned} & 230 \mathrm{~V} / 0.5 \mathrm{~A} \\ & 12 \mathrm{Vdc} \\ & 10 \mathrm{~mA} \end{aligned}$ | N/A | $\begin{aligned} & 230 \mathrm{~V} / 0.5 \mathrm{~A} \\ & 12 \mathrm{Vdc} \\ & 10 \mathrm{~mA} \end{aligned}$ | N/A |

Table 50
$I_{\max } \quad$ The maximum value of current that the SPD can withstand and remain operational.
$I_{n} \quad$ The nominal value of current that the SPD can withstand at least 20 times and still be serviceable.
$U_{p} \quad$ The residual voltage that is measured across the terminal of the SPD when In is applied.
$U_{c}^{p} \quad$ The maximum voltage which may be continuously applied to the SPD without conducting.
$U_{\text {oc }} \quad$ Open circuit voltage under test conditions.
$I_{s c} \quad$ Short circuit current under test conditions.
$U_{n} \quad$ The nominal rated voltage of the installation
MOV Metal Oxide Varistor
SPD Surge Protective Device.

## Surge Protection Devices

How to choose your surge protection device
The choice of surge protection device depends on your supply arrangements and level of protection required

| Earthing system | Type of protection |  | Connection | Products to be used in a Single phase installation | Three phase installation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TN-C <br> TN-C-S <br> (P-M-E) | Translent voltage surges ( $8 / 20 \mathrm{~ms}$ ) | Class II main protection Imax = 40kA or 15 kA (depending on selection) | Parallel |  |  |
|  |  | Class II fine protection Up < 1kv | Parallel | SPN208S |  |
| $\begin{aligned} & \text { TN-S } \\ & \text { TT } \end{aligned}$ | Translent voltage surges ( $8 / 20 \mathrm{~ms}$ ) | Class II main protection Imax $=15 \mathrm{kA}$ $\operatorname{Imax}=15 \mathrm{kA}$ | Parallel |  | $1 \text { X SPN415D/SPN415R }$ |
|  |  | Class II fine protection Up < 1kv | Parallel | SPN208S |  |

## Connections

SPN140D


SPN215D/R


SPN415D/R


SPN208S

Motor Starters

## Technical Specifications

Electrical Characteristics

- Electrical supply: 230V/400V
- Ambient temperature range:
$-25^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$
- Working life: 100,000 operations AC-3
- Maximum of 40 operations/hour
- Tropicalized for all climates
- Connection with clamp type, terminals connection capacity: Flexible : 1 to 4 N
Rigid : 1.5 to 6 N


## Electrical Connection Single Phase



Fig 41
Time / Current Characteristics


Fig 42



[^0]:    MZN175

[^1]:    Table 26

